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DEVELOPMENT OF AN AIRCRAFT MANEUVER
LOAD SPECTRUM BASED ON VGH DATA

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JULY 1980

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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes a procedure whereby a full scale aircraft maneuver load fatigue spectrum can be developed from recorded VGH data. It is assumed in this development that the internal loads (stresses) at the appropriate control points are available for combinations of velocity, load factor, altitudes and weight so that an interpolation on these points will provide the desired accuracy. The procedure will generate (for a control point) the cumulative probability of exceeding a given stress, exceedances per hour of a given | | |

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stress level, the probability density function for stress and the stress spectrum. The aircraft spectrum is derived from the assumption that the aircraft test loads derived from a linear combination of balanced loading conditions will provide a good simulation of the stress history at and "between" the control points. The application of the program to new designs (mission analysis) and to tracking can be made without modification. The computer program for this calculation is included along with a sample problem. As an example of an application of this program, the stress exceedance functions for a control point on the wing of the F-4 are shown that were computed from the VGII data accumulated over a period of one year.

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FOREWARD

This report was prepared by John W. Lincoln, Structures Division of the Directorate of Flight Systems Engineering. The work was done as a research and development task to assist in the spectrum development work for the F-4 durability and damage tolerance assessment.

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LIST OF SYMBOLS

| | |
|-------------|---|
| N_{v_i} | The number of indicated airspeed intervals in the VGH histogram |
| N_{n_z} | The number of normal load factor intervals in the VGH histogram |
| N_h | The number of altitude intervals in the VGH histogram |
| N_w | The number of weight intervals in the VGH histogram |
| v_i | Indicated airspeed for the VGH histogram intervals |
| n_{z_i} | Normal load factor for the VGH histogram intervals |
| h_i | Altitude for the VGH histogram intervals |
| w_i | Aircraft weight for the VGH histogram intervals |
| H_j | The VGH histogram |
| N_t | The total number of load occurrences in the VGH histogram |
| P_j | The joint probability density function derived from the VGH histogram |
| $N_{v_i}^R$ | The number of intervals in a refinement of an indicated airspeed interval in the VGH histogram |
| $N_{n_z}^R$ | The number of intervals in a refinement of a normal load factor interval in the VGH histogram |
| N_h^R | The number of intervals in a refinement of an altitude interval in the VGH histogram |
| N_w^R | The number of intervals in a refinement of a weight interval in the VGH histogram |
| V_i | A surface, the ordinates of which are indicated airspeeds for determining the stress at a control point |
| N_z | A surface, the ordinates of which are normal load factors for determining the stress at a control point |

| | |
|------------------|---|
| H | A surface, the ordinates of which are altitudes for determining the stress at a control point |
| W | A surface, the ordinates of which are weights for determining the stress at a control point |
| \hat{P}_J | The joint probability density function for the refined VGH histogram |
| N_p | The number of control points on the aircraft structure used in the derivation of the fatigue spectrum |
| P_{ψ}^a | The cumulative probability for the stress at the ath control point |
| $P_{D_{\psi}}^a$ | The probability density function for the stress at the ath control point |
| A_{cb}^a | The stress for the ath load level at the bth point in the sky and the cth control point |
| r_c^a | The fatigue test stress for the ath load level and the cth control point |
| α^{ab} | Scaling coefficients for the ath load level and the bth point in the sky |
| ϕ^a | A surface (generated from the surface P_J) from which P_{ψ}^a can be determined for ath control point |
| ψ^a | The stress surface for the ath control point |
| S^a | A set of ordinates of the graph $1 - P_{\psi}^a$ |
| $S^a(i)$ | The ith member of S^a |

SECTION I

INTRODUCTION

In the application of the mission analysis required by MIL-A-008866A (USAF) to fighter and attack aircraft a problem arises in the selection of the point in the sky (velocity, altitude, and weight) for the load factor spectrum for the combat segment of the mission. It can be shown that in many cases important differences in the spectrum can be obtained from two "reasonable" point selections.

The problem has been particularly severe on some existing aircraft in that a ten percent shift in the stress spectrum can produce a factor of two change in life. Therefore, when it is considered that essentially all of the fatigue damage for fighter and attack aircraft is done in the combat segment, this part of the mission deserves special attention.

From an examination of available VGH data, it is evident that in both the air-to-air and air-to-ground operations a fairly wide variation in velocity, altitude, and weight is observed. Therefore, it would be surprising if a single point in the sky would provide an accurate prediction of the stress spectrum for a control point. This is even more evident for those aircraft which experience non-linearities in the aerodynamic data (i.e., tip stall).

One possible solution is to use multiple points in the sky for this calculation. This can be effectively accomplished by taking the points in the sky and their relative frequency of occurrence that are obtained from that portion of the fleet that is equipped with multichannel recorders (twenty percent of the fleet, which is consistent with current policy, is believed to be an adequate sample). This can be done by taking the VGH histogram (the relative frequency of airspeed, normal load factor, altitude, and weight) and dividing by the total number of load occurrences to obtain the probability that a load will occur in a given interval of airspeed, normal load factor, altitude, and weight. A stress level is selected and a summation is made for each such probability where the corresponding stress at the midpoint of the interval of airspeed, etc, is greater than the selected stress level. This computation produces the cumulative probability of exceeding a stress level. Since the intervals used for the data collection were not designed for this calculation, a provision is made to subdivide the intervals to improve the accuracy of the calculation. This technique is explained in Section III. From the cumulative

probability, the number of stress exceedances per hour, the probability density function, and the stress spectrum can be obtained.

Having the functions referred to above for a number of control points that is adequate to cover the aircraft structure (this number may have to be obtained by trial and error), one may generate the full scale aircraft spectrum by assuming that an arbitrary loading at the control points of the structure can be derived from a linear combination of the loading imposed by balanced load conditions. If N_p control points are used, then N_p balanced load conditions are used to represent the control point load. The use of "representative" balanced load conditions should provide a satisfactory interpolation between control points. These intermediate points should be spot checked against the true spectrum to see if the control point coverage is adequate.

Of course, for a new design, the VGH data does not exist and consequently direct application of this method is impossible. In some cases it will be possible to overcome this difficulty by taking existing VGH data from older aircraft and by use of judgement adapt it to this procedure. In any event, the method should be applied when the proper data becomes available so that by suitable tests and analysis the appropriate changes may be made in the aircraft life predictions.

One important application of this procedure is fighter/attack tracking. The unusual technique is to use the fleet counting accelerometer data and compute the stress for a single point in the sky that is believed to be representative of the particular mission flown (i.e., air-to-air or air-to-ground). In lieu of this approach, one could compute from the VGH data the conditional probability of exceeding a stress given the normal load factor. If this function were available, it would be possible to track to any desired probability on even multiple probability levels depending on what results are desired. This function can be generated from this program by setting all occurrences equal to zero except those that fall in the desired load factor interval. The high positive and low negative load factors may require an extrapolation from neighboring load factors because there may be too few data points to adequately describe these functions.

The program that is discussed in this report is based on the load occurrences in the VGH histogram being dependent on indicated airspeed, normal load factor, altitude, and weight. The stress function is based on the same quantities. An immediate alternate that is

included is to use equivalent load factor instead of load factor. This removes the weight dependency and considerably reduces the magnitude of the input. This option is included in the computer program described in the text. Other alternates that could be obtained by a simple modification of the program are listed as follows:

| VGH data based on | Stress function based on |
|--|---|
| 1. Indicated airspeed, normal load factor, altitude, and weight. | Mach no., normal load factor, altitude, and weight. |
| 2. Mach no., normal load factor, altitude, and weight. | Mach no., normal load factor, altitude, and weight. |
| 3. Equivalent airspeed, normal load factor, and weight | Equivalent airspeed, normal load factor, and weight. |

The extension of this program to include other degrees of freedom for the aircraft is immediately evident. The major difficulty is the management of the input data required for the load occurrences and the stress function.

SECTION II

ANALYTICAL DERIVATION OF THE SPECTRUM

The first step in the derivation of the fatigue spectrum is to solve for the stress probability distribution function. This requires that the histogram of occurrences in intervals of indicated airspeed, load factor, altitude, and weight be defined. To do this suppose that each of N_{v_i} , N_{n_z} , N_h , and N_w is a positive integer and

- (1) v_{ij} is a simple graph such that the x-projection of v_{ij} is the set of integers in $[1, N_{v_i} + 1]$ and if i is an integer in $[1, N_{v_i} + 1]$ and $i + 1$ is in $[1, N_{v_i} + 1]$ then the indicated airspeed $v_{ij}(i)$ is less than the indicated airspeed $v_{ij}(i + 1)$
- (2) n_{z_j} is a simple graph such that the x-projection of n_{z_j} is the set of integers in $[1, N_{n_z} + 1]$ and if j is an integer in $[1, N_{n_z} + 1]$ and $j + 1$ is in $[1, N_{n_z} + 1]$ then the normal load factor $n_{z_j}(j)$, is less than the normal load factor $n_{z_j}(j + 1)$
- (3) h_i is a simple graph such that the x-projection of h_i is the set of integers in $[1, N_h + 1]$ and if k is an integer in $[1, N_h + 1]$ and $k + 1$ is in $[1, N_h + 1]$ then the altitude $h_i(k)$, is less than the altitude $h_i(k + 1)$
- (4) w_j is a simple graph such that the x-projection of w_j is the set of integers in $[1, N_w + 1]$ and if m is an integer in $[1, N_w + 1]$ and $m + 1$ is in $[1, N_w + 1]$ the weight $w_j(m)$, is less than the weight $w_j(m + 1)$

Further, suppose H_J is a simple surface such that

$[v_{ii}(i), n_{z_i}(j), h_i(k), w_i(m), H_J(v_{ii}(i), n_{z_i}(j), h_i(k), w_i(m))]$ is a point of H_J only if

- (1) i is in $[1, N_{v_i}]$, j is in $[1, N_{n_z}]$, k is in $[1, N_h]$,
 m is in $[1, N_w]$ and
- (2) $H_J(v_{ii}(i), n_{z_i}(j), h_i(k), w_i(m))$ is the number of "load occurrences" in the rectangular interval
 $[v_{ii}(i), v_{ii}(i+1); n_{z_i}(j), n_{z_i}(j+1); h_i(k), h_i(k+1); w_i(m), w_i(m+1)]$
and these load occurrences are assumed to be uniformly distributed within the rectangular interval.

The surface H_J is called the VGH histogram for v_{ii} , n_{z_i} ,
 h_i , and w_i .

The total number of load occurrences included in the VGH histogram H_J is

$$N_t = \sum_{i=1}^{N_{v_i}} \sum_{j=1}^{N_{n_z}} \sum_{k=1}^{N_h} \sum_{m=1}^{N_w} H_J(v_{ii}(i), n_{z_i}(j), h_i(k), w_i(m))$$

Therefore, by definition, the probability that the indicated airspeed, normal load factor, altitude, and weight is in the rectangular interval $[v_{ii}(i), v_{ii}(i+1); n_{z_i}(i), n_{z_i}(j+1); h_i(k), h_i(k+1); w_i(m), w_i(m+1)]$ is

$$P_J(i, j, k, m) = \frac{H_J(v_{ii}(i), n_{z_i}(j), h_i(k), w_i(m))}{N_t}$$

Now suppose that if i is in $[1, N_{V_i} - 1]$ then the interval $[v_{ii}(i), v_{ii}(i + 1)]$ is covered by $N_{V_i}^R$ equal intervals, if j is in $[1, N_{n_z} - 1]$ then $[n_{z_i}(j), n_{z_i}(j + 1)]$ is covered by $N_{n_z}^R$ equal intervals, if k is in $[1, N_h - 1]$ then $[h_i(k), h_i(k + 1)]$ is covered by N_h^R equal intervals, and if m is in $[1, N_w - 1]$ then $[w_i(m), w_i(m + 1)]$ is covered by N_w^R equal intervals.

Since it was supposed that the load occurrences are within the rectangular interval $[v_{ii}(i), v_{ii}(i + 1); n_{z_i}(j), n_{z_i}(j + 1); h_i(k), h_i(k + 1); w_i(m), w_i(m + 1)]$ then the probability that the indicated airspeed, normal load factor, altitude, and weight is in the rectangular interval

$$\begin{aligned} & [v_{ii}(i), v_{ii}(i) + \frac{v_{ii}(i + 1) - v_{ii}(i)}{N_{V_i}^R}; \\ & n_{z_i}(j), n_{z_i}(j) + \frac{n_{z_i}(j + 1) - n_{z_i}(j)}{N_{n_z}^R}; \\ & h_i(k), h_i(k) + \frac{h_i(k + 1) - h_i(k)}{N_h^R}; \\ & w_i(m), w_i(m) + \frac{w_i(m + 1) - w_i(m)}{N_w^R}] \end{aligned}$$

is

$$\hat{P}_J(i, j, k, m) = \frac{H_J(v_{ii}(i), n_{z_i}(j), h_i(k), w_i(m))}{N_t N_{V_i}^R N_{n_z}^R N_h^R N_w^R}$$

(1) Now suppose that V_i is a simple surface such that the x-y projection of V_i is the set of integers in the rectangular

interval $[1, N_{v_i} + 1; 1, N_{v_i}^R]$ and if i and $i + 1$ are integers

in $[1, N_{v_i} + 1]$ and i_R is an integer in $[1, N_{v_i}^R]$ then

$$v_i(i, i_R) = v_{ii}(i) + \left(\frac{i_R - 0.5}{N_{v_i}^R} \right) (v_{ii}(i + 1) - v_{ii}(i))$$

- (2) N_z is a simple surface such that the x - y projection of N_z is the set of integers in the rectangular interval $[1, N_{n_z} + 1; 1, N_{n_z}^R]$ and if j , and $j + 1$ are integers in

$[1, N_{n_z} + 1]$ and j_R is an integer in $[1, N_{n_z}^R]$ then

$$N_z(j, j_R) = n_{z_i}(j) + \left(\frac{j_R - 0.5}{N_{n_z}^R} \right) (n_{z_i}(j + 1) - n_{z_i}(j))$$

- (3) H is a simple surface such that the x , y projection of H is the set of integers in the rectangular interval $[1, N_h + 1; 1, N_h^R]$ and if k and $k + 1$ are integers in $[1, N_h + 1]$ and

k_R is an integer in $[1, N_h^R]$ then

$$H(k, k_R) = h_i(k) + \left(\frac{k_R - 0.5}{N_h^R} \right) (h_i(k + 1) - h_i(k))$$

- (4) W is a simple surface such that the x , y projection of W is the set of integers in the rectangular interval $[1, N_w + 1; 1, N_w^R]$ and if m and $m + 1$ are integers in $[1, N_w + 1]$

and m_R is an integer in $[1, N_w^R]$ then

$$W(m, m_R) = w_i(m) + \left(\frac{m_R - 0.5}{N_w^R} \right) (w_i(m + 1) - w_i(m))$$

The assumption is made that the stress at a point in the structure depends only on the indicated airspeed, normal load factor, altitude and weight. Therefore, if it is supposed that each of a and N_p is a positive integer such that a is in $[1, N_p]$

and ψ^a is a simple surface such that $(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R))$, $\psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R))$ is a point of ψ^a only if i is in $[1, N_{V_i} + 1]$, i_R is in $[1, N_{V_i}^R]$, \dots, m is in $[1, N_w + 1]$, m_R is in $[1, N_w^R]$ and $\psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R))$ is the stress for the a th control point corresponding to the indicated airspeed $V_i(i, i_R)$, the normal load factor $N_z(j, j_R)$, the altitude $H(k, k_R)$, and the weight $W(m, m_R)$.

The surfaces ψ^a and \hat{P}_j are used in the calculation of the cumulative probability of exceeding a given stress as follows: Suppose that N_{Γ_L} is a positive integer and Γ_L is a uniformly increasing sequence with x -projection $[1, N_{\Gamma_L}]$ and ϕ^a is a simple surface such that

$$(1) \quad \phi^a(i, j, k, m, i_R, j_R, k_R, m_R) = \hat{P}_j(i, j, k, m) \\ \text{if } \psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R)) > \Gamma_L(b)$$

$$(2) \quad \phi^a(i, j, k, m, i_R, j_R, k_R, m_R) = 0 \\ \text{if } \psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R)) \leq \Gamma_L(b)$$

Therefore, the probability that the stress is greater than $\Gamma_L(b)$ is

$$P_{\psi^a}(\Gamma_L(b)) = \sum_{i=1}^{N_{V_i}} \sum_{j=1}^{N_{n_z}} \sum_{k=1}^{N_h} \sum_{m=1}^{N_w} \sum_{i_R=1}^{N_{V_i}^R} \sum_{j_R=1}^{N_{n_z}^R} \sum_{k_R=1}^{N_h^R} \sum_{m_R=1}^{N_w^R} \\ \phi^a(i, j, k, m, i_R, j_R, k_R, m_R)$$

The probability density function $P_{D_{\psi^a}}$ is the derivative of the cumulative probability function P_{ψ^a} . This derivative is computed as follows: Suppose a is an integer in $[1, N_p]$ and that ζ^a is a simple graph with x -projection the interval $[1, N_{\Gamma_L}]$ such that

(1) if b is an integer in $[1, N_{\Gamma_L}]$ then $\zeta^a(b) = P_{D_\Psi}a(b)$ and

(2) if c is a number in $[b, b + 2]$ there exists a $u_1, u_2,$
and u_3 such that $\zeta^a(c) + u_1c^2 + u_2c + u_3$ where $u_1, u_2,$
 u_3 are determined from the equations

$$\begin{aligned}\zeta^a(b) &= b^2 & b & 1 & u_1 \\ \zeta^a(b+1) &= (b+1)^2 & (b+1) & 1 & u_2 \\ \zeta^a(b+2) &= (b+2)^2 & (b+2) & 1 & u_3\end{aligned}$$

Therefore

(1) if $b = 1$

$$P_{D_\Psi}a(1) = 2u_1 \Gamma_L(1) + u_2$$

$$P_{D_\Psi}a(2) = 2u_1 \Gamma_L(1) + u_2$$

(2) if b is in $[2, N_{\Gamma_L} - 3]$

$$P_{D_\Psi}a(b+1) = 2u_1 \Gamma_L(b+1) + u_2$$

(3) if $b = N_{\Gamma_L} - 2$

$$P_{D_\Psi}a(N_{\Gamma_L} - 1) = 2u_1 \Gamma_L(N_{\Gamma_L} - 1) + u_2$$

$$P_{D_\Psi}a(N_{\Gamma_L}) = 2u_1 \Gamma_L(N_{\Gamma_L}) + u_2$$

The next step in the derivation of the fatigue loading spectrum is to determine the stress and the frequency of that stress in the spectrum. This is done by an indirect process as shown below. Suppose that the fatigue test spectrum is to be composed of N cycles at M stress levels. Further, suppose that a is a positive integer in $[1, N_p]$ and S^a is a sequence of M numbers such that $s^a(i)$ and $s^a(j)$ are members of S^a only if $0 < s^a(i) < s^a(j) < 1$ and $i < j$.

Therefore, each member of S^a corresponds to an ordinate of the graph $1-P_\psi a$. The M abscissas corresponding to these M ordinates are defined as the M stress levels of the spectrum for the a th control point. The graph $1-P_\psi a$ is known at N_{Γ_L} points. Consequently, an approximation to $1-P_\psi a$ must be found in order to compute the spectrum stress levels. Suppose β is a simple graph with x -projection the interval $[\Gamma_L(1), \Gamma_L(N_{\Gamma_L})]$ and if k is in $[1, N_{\Gamma_L}]$ then $\beta(\Gamma_L(k)) = 1-P_\psi a(\Gamma_L(k))$. Further, suppose that if $i-1, i$, and $i+1$ are in $[1, N_{\Gamma_L}]$, δ_L is $\Gamma_L(k+1) - \Gamma_L(k)$, and x is in $[-\delta_L, \delta_L]$ then

$$\beta(x + \Gamma_L(k)) = [1 \frac{x}{\delta_L} (\frac{x}{\delta_L})^2] \begin{bmatrix} 0 & 1 & 0 \\ -\frac{1}{2} & 0 & \frac{1}{2} \\ \frac{1}{2} & -1 & \frac{1}{2} \end{bmatrix} \begin{bmatrix} \beta(\Gamma_L(k-1)) \\ \beta(\Gamma_L(k)) \\ \beta(\Gamma_L(k+1)) \end{bmatrix}$$

It follows then that if i is in $[1, M]$ there exists an integer k such that $P_\psi a(\Gamma_L(k-1)) \leq s^a(i) \leq P_\psi a(\Gamma_L(k))$ and a number x such that $\beta(x + \Gamma_L(k)) = s^a(i)$. The number x is obtained from a solution of a quadratic equation and $x + \Gamma_L(k)$ is the stress corresponding to $s^a(i)$.

The fraction of the N cycles, n_i , that are associated with the i th stress level is defined as follows:

$$n_1 = \frac{s(1) + s(2)}{2}$$

$$n_i = \frac{s(i+1) - s(i-1)}{2} \quad 1 < i < M$$

$$n_M = 1 - \frac{(s(M) + s(M-1))}{2}$$

It follows then that if i is in $[1, M]$ and if the sequence S^a is used for each of the control points then there will be an equal number of loading cycles for the i th load level for each of the control points.

The final step is to determine a set of coefficients which when multiplied by the stresses corresponding to balanced load conditions for the aircraft will produce the desired stress levels at the aircraft control points. Suppose a is a positive integer in $[1, M]$, b is a positive integer in $[1, N_p]$, and c is a positive integer in $[1, N_p]$. Therefore, if A_{cb}^a is the stress for the a th load level at the b th point in the sky and the c th control point and r_c^a is the stress desired in the fatigue test for the a th load level and the c th control point then there exists a set of coefficients α_{ab} such that $r_c^a = A_{cb}^a \alpha_{ab}$.

SECTION III

DESCRIPTION OF THE COMPUTER PROGRAM

1 NOTATION

The right hand side of the following relations are defined in Section II.

$$NT421 = N_{v_i}$$

$$NT422 = N_{n_z}$$

$$NT423 = N_h$$

$$NT424 = N_w$$

$$NT = N_t$$

$$PJT = \hat{P}_j$$

$$NRVI = N_{v_i}^R$$

$$NRNZ = N_{n_z}^R$$

$$NRH = N_h^R$$

$$NRW = N_w^R$$

$$VII = v_{ii}$$

$$NZI = n_{z_i}$$

$$HI = h_i$$

$$WI = w_i$$

$$VI = v_i$$

$$NZ = N_z$$

$$H = H$$

$$W = W$$

$$NPS = N_p$$

$$PPSI = P_\psi a \text{ (The } a \text{ is not explicitly identified in the program)}$$

$$PDPSI = P_{D_\psi} a \text{ (The } a \text{ is not explicitly identified in the program)}$$

$$PS = A$$

$PLD = \Gamma$
 $\text{ALPHA} = \alpha$
 $FVI = v_{ii}(N_{v_i} + 1)$
 $FNZ = n_{z_i}(N_{n_z} + 1)$
 $FH = h_i(N_h + 1)$
 $FW = w_i(N_w + 1)$
 $\text{FACTOR} - \text{Stress scaling factor. FACTOR} = 1 \text{ unless otherwise specified.}$
 $\text{HOURS} - \text{The number of hours of data in the VGH histogram}$
 $PSIL = \Gamma_L$
 $\text{AREAN} = s^a$
 $\text{DELTA} = \delta_L$
 $\text{APDPSI}(I) = 1.0 - PPSI(I)$
 $\text{PSILL}(I) - \text{The stress level that is the abscissa of the point of PPSI whose ordinate is AREAN}(I)$
 $\text{FRAC}(I) - \text{The fraction of the total number of cycles in the spectrum that correspond to PSILL}$
 $NPSIL = N_{\Gamma_L}$
 $NPSILL = M$
 $\text{EXCEED}(I) - \text{The number of exceedances per hour of the stress PSIL}(I)$
 $\text{NZERO} - \text{Control number to zero the input numbers at the start of a run and then prevent them from being zeroed between cases}$
 $\text{NPSCT} - \text{Control number for counting the number of control points for which a spectrum has been computed in a single run}$

2 INTERPOLATION PROCEDURE

Since the stress is initially calculated for only a finite set of points on the stress surface, an assumption must be made to determine the stress for a given indicated airspeed, normal load factor, altitude, and weight. Specifically, the problem may be expressed as follows: Given that NT421, NT422, NT423, NT424, NRV1, NRNZ, NRH, and NRW is a positive integer and I is in [1,NT421], J is in [1,NT422], K is in [1,NT423], M is in [1,NT424], IR is in [1,NRV1], JR is in [1,NRNZ], KR is in [1,NRH], MR is in [1,NRW] and a is in [1,N_p] it is required to create an approximation in the form

$\xi^a(I, J, K, M, IR, JR, KR, MR) =$

$\Xi^a(VI(I, IR), NZ(J, JR), H(K, KR), W(M, MR))$

for the stress as expressed by

$\psi^a(I, J, K, M, IR, JR, KR, MR) =$

$\Psi^a(VI(I, IR), NZ(J, JR), H(K, KR), W(M, MR))$

where Ξ^a is a ruled surface based on $2^4 = 16$ points of Ψ^a . The method of choosing these 16 points and the calculation of the stress approximation is described below.

The first step is to define the function TABLE which contains the projections and ordinates of the Ψ^a surface.

Suppose each of NTAB1, NTAB2, NTAB3, and NTAB4 is a positive integer and that

$$NN12 = NTAB1 + NTAB2$$

$$NN13 = NN12 + NTAB3$$

$$NN14 = NN13 + NTAB4$$

$$NP = NTAB1 \cdot NTAB2 \cdot NTAB3 \cdot NTAB4$$

$$NF = NN14 + NP$$

Further, suppose that TABLE is a simple graph such that the x-projection of TABLE is the set of integers in the interval [1, NF] and each of I1, I2, I3, and I4 is a positive integer.

Also,

- (1) if I1 and I1 + 1 are in [1, NTAB1] then the indicated airspeed TABLE (I1) is less than the indicated airspeed TABLE (I1 + 1)
- (2) if I2 and I2 + 1 are in [NTAB1 + 1, NN12] then the normal load factor TABLE (I2) is less than the normal load factor TABLE (I2 + 1)
- (3) if I3 and I3 + 1 are in [NN12 + 1, NN13] then the altitude TABLE (I3), is less than the altitude TABLE (I3 + 1)
- (4) if I4 and I4 + 1 are in [NN13 + 1, NN14] then the weight TABLE (I4) is less than the weight TABLE (I4 + 1)
- (5) if I1 is in [1, NTAB1], I2 is in [NTAB1 + 1, NN12], I3 is in [NN12 + 1, NN13], I4 is in [NN13 + 1, NN14]

and n is in $[NN14 + 1, NF]$ and is equal to $NN14 + (I4 - NN13 - 1) \cdot NTAB3 \cdot NTAB2 \cdot NTAB1 + (I3 - NN12 - 1) \cdot NTAB2 \cdot NTAB1 + (I2 - NTAB1 - 1) \cdot NTAB1 + I1$ then the stress TABLE (n) is the stress that corresponds to the indicated airspeed TABLE (I1), the normal load factor TABLE (I2), the altitude TABLE (I3) and the weight TABLE (I4).

The positive integers I1, I2, I3, and I4 are determined as follows: A search is made for the integer i that will determine the smallest number TABLE (i) that equals or exceeds $VI(I, IR)$. If $i = 1$ satisfies this requirement then I1 is set equal to 2. If i is in $[2, NTAB1]$ then I1 is set equal to i . If no i can be found in $[2, NTAB1]$ then I1 is set equal to $NTAB1$. A search is made for the integer j that will determine the smallest number TABLE (j) that equals or exceeds $(NZ(J, JR))$. If $j = NTAB1 + 1$ then I2 is set equal to $NTAB1 + 2$. If j is in $[NTAB1 + 2, NN12]$ then I2 is set equal to j . If no j can be found to satisfy the requirement then I2 is set equal to $NN12$. Also, a search is made for the integer k that will determine the smallest number TABLE (k) that equals or exceeds $H(K, KR)$. If $k = NN12 + 1$ then I3 is set equal to $NN12 + 2$. If k is in $[NN12 + 2, NN13]$ then I3 is set equal to k . If no k can be found in $[NN12 + 2, NN13]$ then I3 is set equal to $NN13$. A final search is made for the integer m that will determine the smallest number TABLE (m) that equals or exceeds $W(M, MR)$. If $m = NN13 + 1$ then I4 is set equal to $NN13 + 2$. If m is in $[NN13 + 2, NN14]$ then I4 is set equal to m . If no m can be in $[NN13 + 2, NN14]$ then I4 is set equal to $NN14$.

The next step is to identify the integers required for the final calculations.

With

$$\begin{aligned} NP12 &= NTAB1 \cdot NTAB2 \\ NP13 &= NP12 \cdot NTAB3 \end{aligned}$$

these are:

$$\begin{aligned} N2222 &= NN14 + (I4 - NN13 - 1) \cdot NP13 + (I3 - NN12 - 1) \cdot \\ &\quad NP12 + (I2 - NTAB1 - 1) \cdot NTAB1 + I1 \\ N1222 &= N22 - 1 \\ N2122 &= N222 - NTAB1 \\ N1122 &= N2122 - 1 \\ N2212 &= N2222 - NP12 \end{aligned}$$

$N1212 = N2212 - 1$
 $N2112 = N2212 - NTAB1$
 $N1112 = N2112 - 1$
 $N2221 = N222 - NP13$
 $N1221 = N2221 - 1$
 $N2121 = N2221 - NTAB1$
 $N1121 = N2121 - 1$
 $N2211 = N2221 - NP12$
 $N1211 = N2211 - 1$
 $N2111 = N2211 - NTAB1$
 $N1111 = N2111 - 1$

Therefore, if

$$X1RAT = \frac{VI(I, IR) - TABLE(I1-1)}{TABLE(I1) - TABLE(I1-1)}$$

$$X2RAT = \frac{NZ(J, JR) - TABLE(I2-1)}{TABLE(I2) - TABLE(I2-1)}$$

$$X3RAT = \frac{H(K, KR) - TABLE(I3-1)}{TABLE(I3) - TABLE(I3-1)}$$

$$X4RAT = \frac{W(M, MR) - TABLE(I4-1)}{TABLE(I4) - TABLE(I4-1)}$$

then

$$\begin{aligned} AMP111 &= TABLE(N1111) + X1RAT(TABLE(N2111) - TABLE(N1111)) \\ AMP211 &= TABLE(N1211) + X1RAT(TABLE(N2211) - TABLE(N1211)) \\ AMP121 &= TABLE(N1121) + X1RAT(TABLE(N2121) - TABLE(N1121)) \\ AMP221 &= TABLE(N1221) + X1RAT(TABLE(N2221) - TABLE(N1221)) \\ AMP112 &= TABLE(N1112) + X1RAT(TABLE(N2112) - TABLE(N1112)) \\ AMP212 &= TABLE(N1212) + X1RAT(TABLE(N2212) - TABLE(N1212)) \\ AMP122 &= TABLE(N1122) + X1RAT(TABLE(N2122) - TABLE(N1122)) \\ AMP222 &= TABLE(N1222) + X1RAT(TABLE(N2222) - TABLE(N1222)), \end{aligned}$$

$$AMP11 = AMP111 + X2RAT(AMP211 - AMP111)$$

$$AMP12 = AMP112 + X2RAT(AMP212 - AMP112)$$

$$AMP22 = AMP122 + X2RAT(AMP222 - AMP122),$$

$$AMP1 = AMP11 + X3RAT(AMP21 - AMP11)$$

$$AMP2 = AMP12 + X3RAT(AMP22 - AMP12),$$

$$\xi^a (K, J, K, M, IR, JR, KR, MR) = (AMP1 + X4RAT(AMP2 - AMP1)) \cdot FACTOR$$

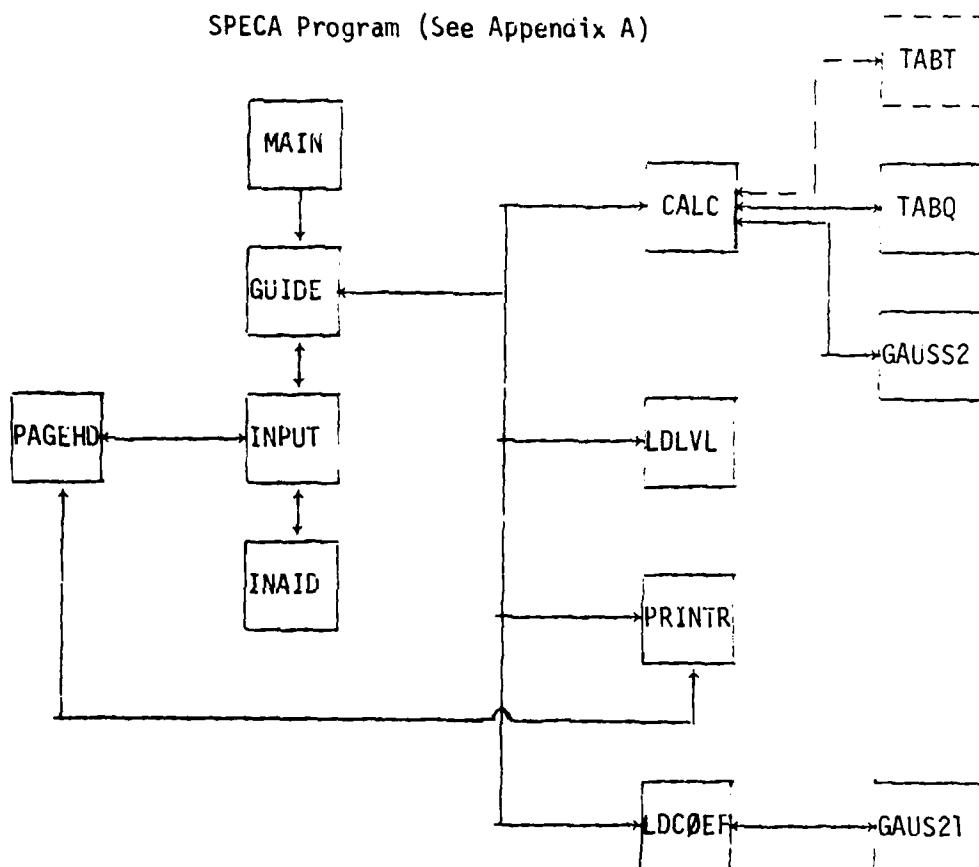
It is seen that the sixteen points on the ψ^a surface are reduced to eight points on the ξ^a surface by an interpolation on the indicated airspeed. The eight points are reduced to four points on the ξ^a surface by an interpolation on the normal load factor. Next, the

four points are reduced to two points on the Σ^3 surface by an interpolation on the altitude, and finally these two points are reduced to the desired stress by an interpolation on the weight.

Note that the number FACTOR is used to scale the calculation made in the table look up routine.

3 COMPUTER FLOW DIAGRAM AND PROGRAM

The computer routine was coded in FORTRAN Extended Language with the main program and subroutines arranged as follows:



MAIN - Main Program - Sets NZERO and NPSCT to zero and transfers program control to GUIDE

GUIDE - Subroutine - Initially zeros input and output numbers and after first case zeros output numbers before the calculations are performed. **GUIDE**, the main controlling subroutine, transfers control to **INPUT**, **CALC**, **LDLVL**, **PRINTR**, and **LDCDEF** in turn.

INPUT - Subroutine - Reads in all input data including the VGH histogram and the stress table. There are two formats for reading in floating point numbers and three formats for reading in fixed point numbers. The details of the data input are discussed later in this section.

INAID - Subroutine - Called by **INPUT** and has the purpose of writing out certain input data.

- (1) NRV_I, NRV_Z, NRH, NRW
- (2) FACT_R
- (3) PSIL
- (4) AREAN
- (5) PS
- (6) Stress table
- (7) VGH histogram table
- (8) FVI, FNZ, FH, FW

Also, **INAID** sets NZERO=1 for control of data handling in **GUIDE**

PAGEHD - Subroutine - Writes out page heading including run identification, date and page number

CALC - Subroutine - Computes PPSI and PDPSI

LDLVL - Subroutine - Computes PSIL and FRAC

LDCDEF - Subroutine - Computer ALPHA

TABQ - Subroutine - Called from **CALC** to perform the interpolation discussed in Section IV, B, that computes the stress corresponding to a given indicated airspeed, normal load factor, altitude, and weight.

TABT - Subroutine - called from **CALC** as an alternate to **TABQ** for the interpolation to compute the stress corresponding to a given indicated airspeed, equivalent normal load factor, and altitude.

GAUSS2 - Subroutine - Called from CALC to solve the simultaneous equations that are required to pass second order equations through the points of PPSI so that the differentiation for PDPSI can be performed. The subroutine uses the Gauss-Jordan method for solving the sets of simultaneous equations.

GAUS21 - Subroutine - Called from LUCDEF and is used to solve the set of equations PLD(I) = PS(K,J) * ALPHA(J). This subroutine is identical to GAUSS2 except for a DIMENSION statement change.

PRINTR - Subroutine - Called from GUIDE to write out computed output data. In particular, PRINTR prints

- (1) PPSI
- (2) EXCEED
- (3) HOURS
- (4) PDPSI
- (5) PSILL, FRAC

4 EQUIVALENCE TABLES

The technique that has been used in coding this routine is to place all input and output numbers in blank common. All input and output floating point numbers are called parameters and are contained in P (dimensioned 10,000). All input and output fixed point numbers are called integers and are contained in NTEGER (dimensioned 100). To make the program more easily interpreted, EQUIVALENCE statements are used to provide the P and NTEGER numbers with more recognizable names. The SPECA program parameter and integer tables are given below.

PARAMETER EQUIVALENCE TABLE

| P | Dimension | Term | P | Dimension | Term |
|---|-----------|---------|------|-----------|--------------|
| 1 | (1) | FMN,FVI | 1201 | (100) | APDPSI(1, |
| 2 | (1) | FNZ | 1300 | | APDPSI(100, |
| 3 | (1) | FH | 1301 | (100) | PSIL(1) |
| 4 | (1) | FW | 1400 | | PSIL(100) |
| 5 | (1) | FACTØR | 1401 | (100) | FRAC(1) |
| 6 | (1) | HOURS | 1500 | | FRAC(100) |
| . | | | 1501 | (100,25) | PLUS(1,1) |
| . | | | 4000 | | PLDS(100,25) |
| . | | | 4001 | (25) | ALPHA(1) |
| . | | | 4025 | | ALPHA(25) |

| P | Dimension | Term | P | Dimension | Term |
|------|-----------|------------|------|-----------|-------------|
| 100 | (1) | NT | . | | |
| 101 | (100) | PSIL(1) | . | | |
| 200 | | PSIL(100) | . | | |
| 201 | (100) | AREAN(1) | 5001 | (25) | VII(1) |
| 300 | | AREAN(100) | 5025 | | VII(25) |
| 301 | (25,25) | PS(1,1) | 5026 | (25) | NZI(1) |
| 925 | | PS(25,25) | 5050 | | NZI(25) |
| . | | | 5051 | (25) | HI(1) |
| . | | | 5075 | | HI(25) |
| . | | | 5076 | (25) | WI(1) |
| 1001 | (100) | PPSI(1) | 5100 | . | WI(25) |
| 1100 | | PPSI(100) | . | | |
| 1101 | (100) | PDPSI(1) | . | | |
| 1200 | | PDPSI(100) | 6001 | (100) | EXCEED(1) |
| | | | 6100 | | EXCEED(100) |

INTEGER EQUIVALENCE TABLE

| NTEGER | Dimension | Term | NTEGER | Dimension | Term |
|--------|-----------|--------|--------|-----------|----------|
| 1 | (1) | IDENT | . | | |
| 2 | . | NPF1 | . | | |
| 3 | . | NPF2 | . | | |
| 4 | . | NPF3 | 56 | (2) | NTB41(1) |
| 5 | | NPF4 | 57 | | NTB41(2) |
| 6 | | NTI4 | 58 | (2) | NTB42(1) |
| 7 | | NTW4 | 59 | | NTB42(2) |
| 8 | | MONTH | 60 | (2) | NTB42(1) |
| 9 | | DAY | 61 | | NTB43(2) |
| 10 | | YEAR | 62 | (2) | NTB44(1) |
| 11 | | NPSIL | 63 | | NTB44(2) |
| 12 | | NPSILL | 64 | (1) | NTB21 |
| 13 | | NPS | 65 | (1) | NTB22 |
| 14 | | NMORE | | | |
| 15 | | NRMN | | | |
| 16 | | NRNZ | | | |
| 17 | | NRH | | | |
| 18 | | NRW | | | |
| 19 | | | | | |
| 20 | | | | | |
| 21 | | NTB | | | |
| . | | | | | |
| . | | | | | |
| 49 | | NPAGE | | | |

5 INPUT DATA

All of the input data described below is read into the program by means of the subroutine INPUT. INPUT is a general purpose subroutine for reading data from cards. For this program, the full capabilities of INPUT are not required and consequently there will be some zeros in the input that serve to bypass certain options.

The following deck arrangement is recommended:

14I5 Format

| | | | | | | | | | | | | | |
|-------|------|---|---|---|------|------|-------|-----|------|------|--------|-----|----|
| IDENT | NPF1 | 0 | 0 | 0 | NT14 | NTW4 | MUNTH | DAY | YEAR | NPSI | NPSIIL | NPS | 21 |
|-------|------|---|---|---|------|------|-------|-----|------|------|--------|-----|----|

7I5 Format

| | | | | | | |
|------|------|-----|-----|---|---|-----|
| NRVI | NRNZ | NRH | NRW | 0 | 0 | NIB |
|------|------|-----|-----|---|---|-----|

72H Format

Run Description

72H Format

Run Description

3I5

| | | |
|---|---|---|
| 1 | 6 | 1 |
|---|---|---|

6E10.3 Format

| | | | | | |
|-----|-----|----|----|--------|-------|
| FVI | FNZ | FH | FW | FACTOR | HOURS |
|-----|-----|----|----|--------|-------|

3I5 Format

| | | |
|-----|-------|---|
| 101 | 100 + | 1 |
|-----|-------|---|

6E10.3 Format

PSIL(1) - PSIL(NPSIL)

3I5 Format

| | | |
|--------|-------|---|
| 201 | 200 + | 1 |
| NPSILL | | |

6E10.3 Format

AREAN(1) - AREAN(NPSILL)

If NPS > 1 go to (a)

If NPS = 0 go to (b)

(a)

3I5 Format

| | | |
|-----|------|---|
| 301 | 300+ | 1 |
| NPS | | |

6E10.3 Format

PS(1,1) - (PS(NPS,1)

3I5 Format

| | | |
|-----|-------|---|
| 326 | 325 + | 1 |
| NPS | | |

6E10.3 Format

PS(1,2) - PS(NPS,2)

3I5 Format

| | | |
|-----|-------|---|
| 351 | 350 + | 1 |
| NPS | | |

6E10.3 Format

| |
|---------------------|
| PS(1,3) - PS(NPS,3) |
|---------------------|

3I5 Format

| | | |
|--------|---------|---|
| 301 + | 300 + | |
| 25(NPS | (NPS-1) | 1 |
| -1) | ·25+NPS | |

6E10.3 Format

| |
|-------------------------|
| PS(1,NPS) - PS(NPS,NPS) |
|-------------------------|

- (b) If NTI4 > 0 go to (c) to read NI14 table(s). For the first run in a computer input the stress table and the VGH histogram table must be read. Subsequent runs may require no new tables (NTI4 = 0), one new table (NTI4 = 1), or two new tables (NTI4 = 2).

If NTI4 = 0 go to (g)

(c)

5I10 Format

| | | | | |
|---|-------|-------|-------|-------|
| I | NTAB1 | NTAB2 | NTAB3 | NTAB4 |
|---|-------|-------|-------|-------|

(Stress table control cards)

6E10.3 Format

TABLE(1) - TABLE(NTAB1)
(indicated airspeeds for the stress table)

6E10.3 Format

TABLE(NTAB1+1) - TABLE(NN12)
(normal load factors for the stress table)

6E10.3 Format

TABLE(NN12+1) - TABLE(NN13)
(altitudes for the stress table)

If NTB = 1 go to (d)

If NTB = 2 go to (e)

(d)

6E10.3 Format

TABLE(NN13+1) - TABLE(NN14)
(weights for the stress table)

6E10.3 Format

TABLE(NN14+1) - TABLE(NF)
(stress amplitudes for the stress table)
(see Section 3.2 for ordering of these entries)

go to (f)

(e)

E10.3 Format

WTTB3

(ref. weight)

6E10.3 Format

TABLE(NN13+1) - TABLE(NF)
(stress amplitudes for the stress table)
(see Section 3.2 for ordering of these entries)

(f)

5I10 Format

| | | | | |
|---|-------|-------|-------|-------|
| 2 | NT421 | NT422 | NT423 | NT424 |
|---|-------|-------|-------|-------|

(VGH histogram control cards)

6E10.3 Format

VII(1) - VII(NT421)
(indicated airspeeds for VGH histogram table)

NZI(1) - NZI(NT422)
(normal load factor for VGH histogram table)

H1(1) - H1(NT423)
(altitudes for VGH histogram table)

W1(1) - W1(NT424)
(weights for VGH histogram table)

$\gamma^a(VII(1),NZI(1),H1(1),W1(1))$ -
 $\gamma^a(VII(NT421),NZI(NT422),H1(NT423),W1(NT424))$
(load occurrences in VGH histogram table)
(see discussion below for ordering of these entries)

(g) END OF FILE

The first card contains 14 fixed point (integer) numbers arranged in 15 fields. These 14 entries in order on this card are

- (1) IDENT - run number
- (2) NPF1 = 3 if $N_p = 1$
= 3 + N_p if $N_p > 1$
- (3) 0
- (4) 0
- (5) 0
- (6) NT14 - the number of quadruple tables to be read (for this count the stress table and the VGH histogram table are each considered quadruple tables.)

- (7) NIW4 = 1 for print of quadruple tables
= 0 otherwise
- (8) MONTH - month in date for page heading
- (9) DAY - day in date for page heading
- (10) YEAR - year in date for page heading
- (11) NPSIL = N_{F_L}
- (12) NPSILL = M
- (13) NPS - The number of control points if $N_p > 1$. NPS = 0
if $N_p = 1$
- (14) 21

The second card contains seven fixed point numbers arranged in 15 fields. In order these entries are

- (1) NRVI = $N_{V_i}^R$
- (2) NRNZ = $N_{n_z}^R$
- (3) NRH = N_h^R
- (4) NRW = N_w^R
- (5) 0
- (6) 0
- (7) NTB = 1 if the load occurrences in the VGH histogram depend on indicated airspeed, normal load factor, altitude, and weight.
NTB = 2 if the load occurrences in the VGH histogram depend on indicated airspeed, equivalent normal load factor, and altitude

The third and fourth cards contain a72H field each for the purpose of run description, etc.

The fifth card contains 1, 6, and 1 in 15 fields

The sixth card contains six floating point numbers arranged in E10.3 fields. These six numbers are placed in the following order:

$$(1) FVI = v_i(N_{V_i} + 1)$$

- (2) FNZ = $n_z(N_{n_z} + 1)$
- (3) FH = $h(N_h + 1)$
- (4) FW = $w(N_w + 1)$
- (5) FACTOR - stress scaling factor
- (6) HOURS - number of hours of data in the VGH histogram

The seventh card contains the three fixed point numbers 101, 100 + NPSIL, 1 in order in 15 fields. NPSIL must not exceed 100.

The next card(s) contains(s) the numbers PSIL(1) through PSIL(NPSIL) in E10.3 fields, six numbers per card.

The next entry contains the fixed point numbers 201, 200 + NPSILL, 1 in order in 15 fields. NPSILL must not exceed 100.

Following this card the floating point numbers AREAN(1) through AREAN(NPSIL), arranged in E10.3 fields, six numbers per card, are entered.

If NPS = 0 then the PS matrix is omitted from the input deck.

If NPS = i then the PS matrix is placed next in the input deck. PS is dimensioned (25,25) and is equivalenced to P such that P(301) = PS(1,1). Therefore, it follows that P(300+NPS) = PS(NPS,i), P(326) = PS(1,2), and P(301+25(NPS-1)) = PS(1,NPS). Consequently the NPS blocks of data are read in as follows:

First block -

The first card contains the fixed point numbers 301, 300+NPS, 1 arranged in 15 fields.

The next entries are the floating point numbers FS(1,1) through FS(NPS,1) in E10.3 fields, six numbers per card.

Second block -

The first card contains the fixed point numbers 326, 325+NPS, 1 arranged in 15 fields.

The next entries are the floating point numbers PS(1,2) through PS(NPS,2) in E10.3 fields, six numbers per card.

.

.

.

Nr'Sth block -

The first card contains the fixed point numbers 301+ 25(NPS-1), 300+(NPS-1)(25) + NPS arranged in 15 fields.

The next entries are the floating point numbers PS(1,NFS) through PS(NPS,NFS) in E10.3 fields, six numbers per card.

The remaining entries are the stress table and the VGH histogram table. These entries are prepared as follows:

If I = 1 then the entry is the stress table where there are $NP = NTAB1 \cdot NTAB2 \cdot NTAB3 \cdot NTAB4$ points defined by NTAB1 indicated airspeeds, NTAB2 normal load factors, NTAB3 altitudes, NTAB4 weights. These points are entered as ordinates of the simple graph TABLE which was defined in paragraph 2 of this section.

The first card for the stress table contains five (5) fixed point numbers in 15 fields in the order

- (1) 1
- (2) NTAB1
- (3) NTAB2
- (4) NTAB3
- (5) NTAB4

The next card(s) contain(s) the indicated airspeeds (floating point numbers) TABLE(1) through TABLE(NTAB1) arranged in E10.6 fields, six numbers per card.

The next entries are the normal load factors TABLE(NTAB1 +1, NN12) (see paragraph 2 for definition of arguments) arranged in E10.3 fields six numbers per card.

Next, the card(s) that contain the altitudes TABLE(NN12+1) through TABLE(NN13) arranged in E10.3 fields, six numbers per card are entered in order.

The next entries depend on the number NTB.

If NTB = 1 the card(s) that contain(s) the weights TABLE(NN13+1) through TABLE(NN14) arranged in E10.3 fields, are entered with six numbers per card.

The next card(s) contain(s) the stresses TABLE(NN14+1) through TABLE(NF) arranged in E10.3 fields, six numbers per card. The ordering of the stresses in this entry is defined in paragraph 2 of this section.

If NTB = 2 a card is entered that contains the reference weight WTTB3 in an E10.3 field.

The next card(s) contain(s) the stresses TABLE(NN13+1) through TABLE(NF) arranged in E10.3 fields, six numbers per card. The number NF must not exceed 2000. The ordering of the stresses in this entry is defined in paragraph 2 of this section.
(Note that NTAB4 = 1 for this case.)

This completes the stress table

If I = 2 then the entry is the VGH histogram table where there are NP24 = NT421 · NT422 · NT423 · NT424 regions defined by NT421 indicated airspeed intervals, NT422 normal load factor intervals, NT423 altitude intervals, and NT424 weight intervals.

The first card for the VGH histogram table contains five fixed point numbers in 15 fields in the order

- (1) 2
- (2) NT421
- (3) NT422
- (4) NT423
- (5) NT424

Following this card are the card(s) with the indicated airspeeds (floating point numbers) VII(1) through VII(NT421) arranged in E10.3 fields, six numbers per card.

The next card(s) contain the normal load factors NZI(1) through NZI(NT422) arranged in E10.3 fields, six numbers per card.

Next are the card(s) that contain the altitudes HI(1) through HI(NT423) arranged in E10.3 fields, six numbers per card.

The weight entries WI(1) through WI(NT424) arranged in E10.3 field, six numbers per card, are next.

The final card(s) in the VGI histogram deck are the load occurrences in regions defined by the indicated airspeeds, normal load factors, altitudes, and weights. If i is in $[1, NP]$ then these entries are $\beta(VII(i), NZI(i), HI(i), WI(i))$ through $\beta(VII(NT421), NZI(NT422), HI(NT423), WI(NT424))$ arranged in E10.3 fields, six numbers per card. If i is in $[1, NT421]$, j is in $[1, NT422]$, k is in $[1, NT423]$, and m is in $[1, NT424]$ then the stress that corresponds to $VII(i)$, $NZI(j)$, $FI(k)$, $WI(m)$ is the $((m-1) \cdot NT421 + NT422 + NT423 + (k-1) \cdot NT421 + NT422 + (j-1) \cdot NT421 + i)$ th entry on these cards. The number $NT421 + NT422 + NT423 + NT424 + NT421 \cdot NT422 \cdot NT423 \cdot NT424$ must not exceed 2000.

6 SAMPLE PROBLEM

A sample run is presented for the purpose of acquainting the user with the input data cards and the output. The data used does not represent any particular aircraft or usage. It is assumed that two control points are sufficient in this case to define the full scale aircraft fatigue spectrum. The input cards are as follows:

| | | | | | | | | | | | | | |
|---|---------|---|---------|---|---------|---|---------|----|---------|----|----|---|----|
| 100 | 5 | 0 | 0 | 0 | 2 | 1 | 3 | 30 | 1973 | 23 | 12 | 2 | 21 |
| 2 | 2 | 2 | 2 | 0 | 0 | 1 | | | | | | | |
| CHECK OUT RUN FOR SPECA PROGRAM | | | | | | | | | | | | | |
| V G H DATA IN TABLE CONTROL POINT NUMBER 1 (REVISION 2) • | | | | | | | | | | | | | |
| 1 | 6 | 1 | | | | | | | | | | | |
| 650.0 | 7.0 | | 40000.0 | | 36000.0 | | 1.0 | | 500.0 | | | | |
| 101 | 123 | 1 | | | | | | | | | | | |
| 20000.0 | 22000.0 | | 24000.0 | | 26000.0 | | 28000.0 | | 30000.0 | | | | |
| 32000.0 | 34000.0 | | 36000.0 | | 38000.0 | | 40000.0 | | 42000.0 | | | | |
| 44000.0 | 46000.0 | | 48000.0 | | 50000.0 | | 52000.0 | | 54000.0 | | | | |
| 56000.0 | 58000.0 | | 60000.0 | | 62000.0 | | 64000.0 | | | | | | |
| 201 | 212 | 1 | | | | | | | | | | | |
| 0.05 | 0.10 | | 0.20 | | 0.25 | | 0.30 | | 0.40 | | | | |
| 0.50 | 0.60 | | 0.70 | | 0.80 | | 0.90 | | 0.95 | | | | |
| 301 | 302 | 1 | | | | | | | | | | | |
| 20000.0 | 35000.0 | | | | | | | | | | | | |

326 327 1
25000.0 30000.0

| | 1 | 3 | 3 | 3 | 3 |
|---------|---------|---------|---------|---------|---------|
| 300.0 | 500.0 | 600.0 | | | |
| 3.0 | 6.0 | 8.0 | | | |
| 5000.0 | 20000.0 | 35000.0 | | | |
| 25000.0 | 30000.0 | 35000.0 | | | |
| 20000.0 | 22000.0 | 25000.0 | 42000.0 | 43000.0 | 46000.0 |
| 55000.0 | 57000.0 | 58000.0 | 17000.0 | 18000.0 | 20000.0 |
| 32000.0 | 34000.0 | 35000.0 | 51000.0 | 53000.0 | 54000.0 |
| 15000.0 | 17000.0 | 18000.0 | 26000.0 | 28000.0 | 29000.0 |
| 41000.0 | 42000.0 | 44000.0 | 24000.0 | 26000.0 | 29000.0 |
| 46000.0 | 47000.0 | 50000.0 | 59000.0 | 61000.0 | 62000.0 |
| 21000.0 | 22000.0 | 24000.0 | 36000.0 | 38000.0 | 39000.0 |
| 55000.0 | 57000.0 | 58000.0 | 19000.0 | 21000.0 | 22000.0 |
| 30000.0 | 32000.0 | 33000.0 | 45000.0 | 46000.0 | 48000.0 |
| 27000.0 | 29000.0 | 32000.0 | 49000.0 | 50000.0 | 53000.0 |
| 62000.0 | 64000.0 | 65000.0 | 24000.0 | 25000.0 | 27000.0 |
| 39000.0 | 41000.0 | 42000.0 | 58000.0 | 60000.0 | 61000.0 |
| 22000.0 | 24000.0 | 25000.0 | 33000.0 | 35000.0 | 36000.0 |
| 48000.0 | 49000.0 | 51000.0 | | | |

| | 2 | 3 | 3 | 3 | 3 |
|---------|---------|---------|--------|--------|--------|
| 350.0 | 450.0 | 550.0 | | | |
| 4.0 | 5.0 | 6.0 | | | |
| 10000.0 | 20000.0 | 30000.0 | | | |
| 30000.0 | 32000.0 | 34000.0 | | | |
| 500.0 | 1000.0 | 600.0 | 1000.0 | 1100.0 | 600.0 |
| 700.0 | 770.0 | 7700.0 | 100.0 | 4000.0 | 600.0 |
| 1000.0 | 100.0 | 1000.0 | 700.0 | 2000.0 | 600.0 |
| 6000.0 | 1000.0 | 4000.0 | 600.0 | 6000.0 | 1000.0 |
| 700.0 | 1000.0 | 6000.0 | 3000.0 | 600.0 | 700.0 |
| 1000.0 | 2000.0 | 500.0 | 4000.0 | 700.0 | 1000.0 |
| 500.0 | 4000.0 | 6000.0 | 700.0 | 7000.0 | 7700.0 |
| 4000.0 | 2000.0 | 700.0 | 500.0 | 3000.0 | 500.0 |
| 1000.0 | 600.0 | 3000.0 | 1000.0 | 500.0 | 5000.0 |
| 700.0 | 4000.0 | 600.0 | 3000.0 | 4000.0 | 400.0 |
| 1000.0 | 100.0 | 500.0 | 5000.0 | 5500.0 | 4000.0 |
| 500.0 | 1000.0 | 700.0 | 500.0 | 5000.0 | 3000.0 |
| 600.0 | 6000.0 | 3000.0 | 2000.0 | 4000.0 | 3000.0 |
| 1000.0 | 2000.0 | 200.0 | | | |

100 0 0 0 1 1 8 30 1973 23 12 2 21

2 2 2 0 0 1

CHECK OUT FOR SPECIA PROGRAM

V G H DATA IN TABLE CONTROL POINT NUMBER 2

1 3 3 3 3

300.0 500.0 600.0

| 3.0 | 6.0 | 8.0 | | | |
|---------|---------|---------|---------|---------|---------|
| 5000.0 | 20000.0 | 35000.0 | | | |
| 25000.0 | 30000.0 | 35000.0 | | | |
| 10000.0 | 20000.0 | 24000.0 | 36000.0 | 39000.0 | 40000.0 |
| 45000.0 | 50000.0 | 53000.0 | 17000.0 | 18000.0 | 20000.0 |
| 25000.0 | 27000.0 | 30000.0 | 51000.0 | 53000.0 | 54000.0 |
| 15000.0 | 17000.0 | 18000.0 | 26000.0 | 28000.0 | 29000.0 |
| 32000.0 | 34000.0 | 36000.0 | 25000.0 | 26000.0 | 27000.0 |
| 42000.0 | 43000.0 | 44000.0 | 55000.0 | 56000.0 | 57000.0 |
| 21000.0 | 22000.0 | 24000.0 | 36000.0 | 38000.0 | 39000.0 |
| 55000.0 | 57000.0 | 58000.0 | 19000.0 | 21000.0 | 22000.0 |
| 30000.0 | 32000.0 | 33000.0 | 45000.0 | 46000.0 | 48000.0 |
| 27000.0 | 29000.0 | 32000.0 | 49000.0 | 50000.0 | 53000.0 |
| 62000.0 | 64000.0 | 65000.0 | 24000.0 | 25000.0 | 27000.0 |
| 39000.0 | 41000.0 | 42000.0 | 58000.0 | 60000.0 | 61000.0 |
| 22000.0 | 24000.0 | 25000.0 | 33000.0 | 35000.0 | 36000.0 |
| 48000.0 | 49000.0 | 51000.0 | | | |

Based on this input the following output listing was obtained.

RUN NO 100 DATE 6/20/1971 PAGE NO 1

CHECK OUT RUN FOR SPECIA PROGRAM
VGM DATA IN TABLE CONTROL POINT NUMBER 1 (REVISION 2)

WISCONSIN SUBDIVISIONS

| | |
|--------|---|
| Kewa 1 | 2 |
| Kewa 2 | 2 |
| Kewa 3 | 2 |
| Kewa 4 | 2 |

LOAD MAGNIFICATION FACTOR = 1,0000

INTERVAL LOAD LEVELS FOR INTEGRATION OF JOINT DENSITY FUNCTION

| | | | | | | | |
|----|------------|----|------------|----|------------|----|------------|
| 1 | 2.0000E+04 | 2 | 2.2000E+04 | 3 | 2.4000E+04 | 4 | 2.6000E+04 |
| 5 | 2.6000E+04 | 6 | 3.0000E+04 | 7 | 3.2000E+04 | 8 | 3.4000E+04 |
| 9 | 3.6000E+04 | 10 | 3.8000E+04 | 11 | 4.0000E+04 | 12 | 4.2000E+04 |
| 13 | 4.4000E+04 | 14 | 4.6100E+04 | 15 | 4.8000E+04 | 16 | 5.0000E+04 |
| 17 | 5.2000E+04 | 18 | 5.4100E+04 | 19 | 5.6000E+04 | 20 | 5.8000E+04 |
| 21 | 6.0000E+04 | 22 | 6.2000E+04 | 23 | 6.4000E+04 | 24 | 0. |

CUMULATIVE AREA'S OF LOAD PROBABILITY DENSITY FUNCTION

| | | | | | | | |
|---|-------------|----|-------------|----|-------------|----|-------------|
| 1 | 2.00 001 02 | 2 | 1.00000E-01 | 3 | 2.00000E-01 | 4 | 2.50000E-01 |
| 5 | 3.00 001 01 | 6 | 4.00000E-01 | 7 | 5.00000E-01 | 8 | 6.00000E-01 |
| 9 | 7.00 001 01 | 10 | 6.00000E-01 | 11 | 9.00000E-01 | 12 | 9.50000E-01 |

PUN NO 100 DATE 8/10/1973

PAGE NO 2

QUADRUPLE TABLE NO. 1

FRT VS VT, N7, M1, W

| | | | |
|---------|--------|---------|---------|
| 300.0 | N7 | 600.0 | 600.0 |
| 3,000.0 | N7 | 6,000.0 | 6,000.0 |
| 30,000. | M | 30,000. | 30,000. |
| 300.0 | N | 20000. | 35000. |
| 25000. | M | 30000. | 35000. |
| | PST | | |
| 20010. | 21100. | 25000. | 30000. |
| 32030. | 44200. | 35100. | 51000. |
| 41000. | 47100. | 46100. | 24000. |
| 21000. | 27000. | 26100. | 36000. |
| 30030. | 37300. | 37100. | 45000. |
| 67030. | 64100. | 65100. | 24000. |
| 22030. | 24100. | 25000. | 31000. |

RUN NO 100 DATE 8/30/1973 PAGE NO 4

| INTERNAL LOAD CUMULATIVE PROBABILITY FUNCTION | | | | | |
|---|-------------|--------------|-------------|--------------|-------------|
| LOAD | CUM PROB | LOAD | CUM PROB | LOAD | CUM PROB |
| 2.46930E+00 | 1.00000E+00 | 2.200000E+00 | 1.00000E+00 | 2.400000E+00 | 1.00000E+00 |
| 2.66944E+00 | 9.41014E-01 | 2.400000E+00 | 9.30656E-01 | 3.000000E+00 | 8.31126E-01 |
| 3.20033E+00 | 6.80719E-01 | 3.400000E+00 | 5.44037E-01 | 3.600000E+00 | 5.22759E-01 |
| 3.80000E+00 | 3.22178E-01 | 4.000000E+00 | 2.44392E-01 | 4.200000E+00 | 1.73864E-01 |
| 4.40000E+00 | 1.14117E-01 | 4.600000E+00 | 7.87654E-02 | 4.800000E+00 | 3.48610E-02 |
| 5.00000E+00 | 1.78710E-02 | 5.200000E+00 | 1.44347E-01 | 5.400000E+00 | 1.40771E-01 |
| 5.40000E+00 | 0. | 5.600000E+00 | 0. | 6.000000E+00 | 0. |
| 6.200000E+00 | 0. | 6.400000E+00 | 0. | 6.400000E+00 | 0. |

RUN NO. 100 DATE 8/30/1973 PAGE NO. 5

| CUMULATIVE NUMBER OF EXCEEDANCES PER 1000 HRS | | LOAD | EXCEEDANCES | LOAD | EXCEEDANCES | LOAD | EXCEEDANCES |
|---|--------------|-------------|--------------|-------------|--------------|-------------|-------------|
| 2.00000E+04 | 3.47740E+05 | 2.00000E+04 | 3.45740E+05 | 2.40000E+04 | 3.45740E+05 | 2.80000E+04 | 3.45740E+05 |
| 2.60000E+04 | 3.31775E+05 | 3.20000E+04 | 3.21750E+05 | 3.40000E+04 | 3.21750E+05 | 3.60000E+04 | 3.17522E+05 |
| 3.20000E+04 | 2.31750E+05 | 3.40000E+04 | 1.601025E+05 | 3.60000E+04 | 1.601025E+05 | 4.20000E+04 | 1.61655E+05 |
| 3.80000E+04 | 1.11310E+05 | 4.00000E+04 | 8.43775E+04 | 4.40000E+04 | 8.43775E+04 | 4.80000E+04 | 8.18775E+04 |
| 4.40000E+04 | 4.046250E+04 | 4.60000E+04 | 2.723250E+04 | 5.00000E+04 | 6.37500E+02 | 5.40000E+04 | 6.25190E+01 |
| 5.00000E+04 | 6.162500E+03 | 5.60000E+04 | 0. | 5.11000E+04 | 0. | 6.00000E+04 | 0. |
| 5.60000E+04 | 0. | 6.40000E+04 | 0. | 6.40000E+04 | 0. | 6.00000E+04 | 0. |
| 6.40000E+04 | 0. | | | | | | |

BASED ON 505.00 HOURS

| BUN N# | 100 | DATE | 8/30/1973 | PAGE NO | 6 |
|------------------------------------|---------------|---------------|--------------|--------------|--------------|
| INTERNAL LOAD POSSIBILITY FUNCTION | | | | | |
| LOAD | PCN | PCN | LOAD | PCN | LOAD |
| 2.000000E+04 | 1.95772AF-14 | 2.200000E+04 | 1.552652E-19 | 2.400000E+04 | 6.745227E-06 |
| 2.437130E+04 | 1.731640E-15 | 2.400000E+04 | 3.716743E-05 | 3.000000E+04 | 6.114612E-05 |
| 1.203700E+04 | 7.186190E-05 | 1.400000E+04 | 6.54201E-05 | 3.600000E+04 | 5.546919E-05 |
| 1.030291E+04 | 6.450541E-05 | 4.000000CF+04 | 3.777456E-05 | 4.200000F+04 | 3.155101E-05 |
| 6.462010E+04 | 2.71911E-05 | 4.600000E+04 | 1.974104E-05 | 4.900000E+04 | 1.523546E-05 |
| 5.000000E+04 | 0.7200057F-05 | 5.200000E+04 | 4.410029E-05 | 5.400000E+04 | 4.694674E-05 |
| 5.602100E+04 | 8.710240E-05 | 5.800000E+04 | 0. | 6.000000E+04 | 0. |
| 6.7030005E+04 | 0. | 6.400000E+04 | 0. | | |

RUN NO. 100 DATE 6/30/1971 PAGE NO. 7

REFLCTIC LOADING FRACTIONS

| LOAD | FRACTION | LOAD | FRACTION | LOAD | FRACTION |
|-----------------------------|--------------|--------------|-------------|--------------|-------------|
| 2.76294E+04 | 7.50000E-02 | 2.672792E+04 | 7.50000E-02 | 3.043048E+04 | 7.50000E-02 |
| 3.11111E+04 | 5.00000E-02 | 1.18050F+04 | 7.50000E-02 | 3.317683E+04 | 1.00000E-01 |
| 3.464790E+04 | 0.133000E-01 | 3.644536E+04 | 1.00000E-01 | 3.858916E+04 | 1.00000E-01 |
| 6.120775E+04 | 1.00000E-01 | 4.492567E+04 | 7.50000E-02 | 4.733516E+04 | 7.50000E-02 |
| TOTAL LOAD CYCL S = 172870. | | | | | |

PUN NO 100 DATE 8/18/1973 PAGE NO 8

CHECK OUT FOR OPERA PROGRAM

VGM DATA IN FILE CONTROL POINT NUMBER 2

MICRODATA SURVEYS

NOVY = 2

NONV = 2

NONW = 2

NONW = 2

LOAN MAGNIFICATION FACTOR = 1.0000

INTERPOLAL LOAD LEVELS FOR INTEGRATION OF JOINT DENSITY FUNCTION

| | | | | | | | |
|----|-------------|----|-------------|----|-------------|----|-------------|
| 1 | 2.00E+04 | 2 | 2.20000E+04 | 3 | 2.40000E+04 | 4 | 2.60000E+04 |
| 5 | 2.00E+04 | 6 | 3.00000E+04 | 7 | 3.20000E+04 | 8 | 3.40000E+04 |
| 9 | 3.00E+04 | 10 | 3.20000E+04 | 11 | 3.40000E+04 | 12 | 3.60000E+04 |
| 13 | 4.00E+04 | 14 | 4.80000E+04 | 15 | 4.80000E+04 | 16 | 5.00000E+04 |
| 17 | 5.20000E+04 | 18 | 5.40000E+04 | 19 | 5.60000E+04 | 20 | 5.80000E+04 |
| 21 | 6.00000E+04 | 22 | 6.20000E+04 | 23 | 6.40000E+04 | 24 | 6. |

CUMULATIVE AREAS OF LOAN PROBABILITY DENSITY FUNCTION

| | | | | | | | |
|---|-------------|----|-------------|----|-------------|----|-------------|
| 1 | 5.00000E-01 | 2 | 1.00000E-01 | 3 | 2.00000E-01 | 4 | 2.50000E-01 |
| 5 | 1.00000E-01 | 6 | 6.00000E-01 | 7 | 5.00000E-01 | 8 | 6.00000E-01 |
| 9 | 7.00000E-01 | 10 | 6.00000E-01 | 11 | 9.00000E-01 | 12 | 9.50000E-01 |

प्राचीन विद्या का अध्ययन एवं प्रशिक्षण
परामर्शदाता एवं उत्तम गुणवत्ता वाला

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41

| PUN NO | 106 | DATE | 07/30/1973 | PAGE NO | 10 |
|------------------------|-----|--------|------------|---------|--------|
| QUADRUPLE TARIFF NO. 1 | | | | | |
| PST VS VI, W7, W8, W9 | | | | | |
| VI | | | | | |
| 100.0 | N7 | 009.0 | 600.0 | | |
| 3.0000 | N | 6.0000 | 8.0000 | | |
| 500.0 | N | 2000.0 | 3500.0 | | |
| 2000. | N | 10000. | 35000. | | |
| PST | | | | | |
| 100.0 | | 200.0 | 24000. | 36000. | 19000. |
| 24000. | | 27000. | 31000. | 51000. | 43000. |
| 36000. | | 36000. | 36000. | 54000. | 43000. |
| 100.0 | | 16000. | 25000. | 26000. | 18000. |
| 24000. | | 27000. | 26000. | 27000. | 24000. |
| 36000. | | 36000. | 36000. | 39000. | 36000. |
| 100.0 | | 24000. | 46000. | 46000. | 34000. |
| 24000. | | 37000. | 45000. | 45000. | 32000. |
| 36000. | | 47000. | 47000. | 47000. | 38000. |
| 100.0 | | 65000. | 25000. | 27000. | 49000. |
| 24000. | | 24000. | 31000. | 31000. | 50000. |
| 36000. | | 25000. | 31000. | 31000. | 51000. |
| 100.0 | | 25000. | 31000. | 31000. | 51000. |
| 24000. | | 25000. | 31000. | 31000. | 51000. |
| 36000. | | 25000. | 31000. | 31000. | 51000. |

RIN NO. 100 DATE 6/30/1971 PAGE NO. 11

QUADRUPLE TABLE NO. 2

WISTJ VS VIT, +Z, H, V

VIT = 1500.0 450.0 500.0

4.0000 4.5.0000 6.0010

10000. 20000. 30000.

35000. 40000. 36000.

4500. 1000. 600.

1000. 1500. 2000.

2000. 2500. 3000.

3000. 4000. 5000.

4000. 5000. 6000.

5000. 6000. 7000.

6000. 7000. 8000.

7000. 8000. 9000.

8000. 9000. 10000.

9000. 10000. 11000.

10000. 11000. 12000.

12000. 13000. 14000.

14000. 15000. 16000.

16000. 17000. 18000.

18000. 19000. 20000.

20000. 21000. 22000.

22000. 23000. 24000.

24000. 25000. 26000.

26000. 27000. 28000.

28000. 29000. 30000.

30000. 31000. 32000.

32000. 33000. 34000.

34000. 35000. 36000.

36000. 37000. 38000.

38000. 39000. 40000.

40000. 41000. 42000.

42000. 43000. 44000.

LAST AND CLEAREST IN TABLE 2

VIT = 0.5000000000000000

FV1 = .7010000000000000

FV2 = .4000000000000000

FW = .5000000000000000

FW = .5000000000000000

BIN NO 100 DATE 8/10/1973 PAGE NO 12
 TTFONAL LOAN CUMULATIVE PROBABILITY FUNCTION
 LOAN CUM PROB
 2.00000E+00 1.30000E+00
 2.50000E+00 9.01101E-01
 3.00000E+00 6.11111E-01
 3.50000E+00 3.66667E-01
 4.00000E+00 2.33333E-01
 4.50000E+00 1.46667E-01
 5.00000E+00 8.77778E-02
 5.50000E+00 5.22222E-02
 6.00000E+00 3.00000E-02
 6.40000E+00 1.60000E-02
 6.80000E+00 8.00000E-03
 7.20000E+00 4.00000E-03
 7.50000E+00 2.00000E-03
 7.80000E+00 1.00000E-03
 8.10000E+00 5.00000E-04
 8.40000E+00 2.50000E-04
 8.70000E+00 1.25000E-04
 9.00000E+00 6.25000E-05
 9.30000E+00 3.12500E-05
 9.60000E+00 1.56250E-05
 1.00000E+01 7.81250E-06

RUN NO 100 DATE 8/30/1973 PAGE NO 13

| CUMULATIVE NUMBER OF EXCEEDANCES PEP 1000 MPS | | | |
|---|---------------|--------------|---------------|
| LOAD | EXCEEDANCES | LOAD | EXCEEDANCES |
| 2.000000E+00 | 1.551000E+00 | 2.200000E+00 | 3.557500E+005 |
| 2.400000E+00 | 3.191775E+005 | 2.600000E+00 | 3.217450E+005 |
| 3.100000E+00 | 2.103771E+005 | 3.400000E+00 | 1.801650E+005 |
| 4.100000E+00 | 1.108525E+005 | 4.600000E+00 | 8.276500E+004 |
| 5.400000E+00 | 1.790375E+004 | 6.600000E+00 | 2.261250E+004 |
| 5.000000E+00 | 1.637500E+003 | 5.200000E+00 | 2.625000E+002 |
| 5.400000E+00 | 0. | 5.800000E+00 | 0. |
| 6.200000E+00 | 0. | 6.400000E+00 | 0. |

BASED ON 500,000 HOURS

RUN NO. 100 DATE 8/10/1971 PAGE NO. 16

| INTERNAL LOAD PROBABILITY DENSITY FUNCTION | | LOAD | PROB OF N | LOAD | PROB OF N |
|--|--------------|--------------|--------------|--------------|---------------|
| LOAD | PROB OF N | 2.000000E+04 | 6.562652E-19 | 2.400000E+04 | 6.7465227E-05 |
| 2.45729E-18 | 1.45729E-04 | 2.000000E+04 | 3.739762E-15 | 2.400000E+04 | 6.172227E-05 |
| 2.45729E-18 | 1.73160E-05 | 2.000000E+04 | 5.51711E-05 | 3.000000E+04 | 5.5.1711E-05 |
| 2.45729E-18 | 2.000000E+05 | 2.000000E+04 | 6.58609E-05 | 3.490000E+04 | 3.27279E-05 |
| 3.200000E+04 | 7.25556E-05 | 2.000000E+04 | 3.49714E-05 | 4.200000E+04 | 1.50579E-05 |
| 3.200000E+04 | 8.71604E-05 | 2.000000E+04 | 3.49714E-05 | 4.600000E+04 | 1.50579E-05 |
| 3.200000E+04 | 9.52007E-05 | 2.000000E+04 | 2.01617E-05 | 5.400000E+04 | 1.4941C5E-02 |
| 3.200000E+04 | 1.052007E-05 | 2.000000E+04 | 2.01617E-05 | 6.000000E+04 | 0. |
| 4.400000E+04 | 2.574091E-05 | 2.000000E+04 | 1.1304E2F-06 | 5.400000E+04 | 1.4941C5E-02 |
| 4.400000E+04 | 5.000000E+04 | 2.000000E+04 | 0. | 6.000000E+04 | 0. |
| 5.000000E+04 | 6.767194E-06 | 2.000000E+04 | 0. | 6.000000E+04 | 0. |
| 5.000000E+04 | 4.519292E-04 | 2.000000E+04 | 0. | 6.000000E+04 | 0. |
| 6.200000E+04 | 0. | 2.000000E+04 | 0. | 6.000000E+04 | 0. |

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CYCIC LOADING FRACTIONS

| CYCIC LOAD | FRACTION | LOAD | FRACTION | LOAD | FRACTION |
|-------------|------------------------|-------------|------------------------|-------------|------------------------|
| 2.01245E+04 | 2.5000E-02 | 2.01245E+04 | 7.5000E-02 | 2.01245E+04 | 7.5000E-02 |
| 1.00623E+04 | 1.0000E-01 | 1.00623E+04 | 1.0000E-01 | 1.00623E+04 | 1.0000E-01 |
| 5.03115E+03 | 5.0000E-02 | 5.03115E+03 | 5.0000E-02 | 5.03115E+03 | 5.0000E-02 |
| 2.51578E+03 | 2.5000E-01 | 2.51578E+03 | 2.5000E-01 | 2.51578E+03 | 2.5000E-01 |
| 1.25789E+03 | 1.2500E-02 | 1.25789E+03 | 1.2500E-02 | 1.25789E+03 | 1.2500E-02 |
| 6.28947E+02 | 6.2500E-03 | 6.28947E+02 | 6.2500E-03 | 6.28947E+02 | 6.2500E-03 |
| 3.14474E+02 | 3.1250E-04 | 3.14474E+02 | 3.1250E-04 | 3.14474E+02 | 3.1250E-04 |
| 1.57237E+02 | 1.5625E-05 | 1.57237E+02 | 1.5625E-05 | 1.57237E+02 | 1.5625E-05 |
| 7.86189E+01 | 7.8125E-06 | 7.86189E+01 | 7.8125E-06 | 7.86189E+01 | 7.8125E-06 |
| 3.93095E+01 | 3.90625E-07 | 3.93095E+01 | 3.90625E-07 | 3.93095E+01 | 3.90625E-07 |
| 1.96548E+01 | 1.95312E-08 | 1.96548E+01 | 1.95312E-08 | 1.96548E+01 | 1.95312E-08 |
| 9.82744E+00 | 9.76562E-09 | 9.82744E+00 | 9.76562E-09 | 9.82744E+00 | 9.76562E-09 |
| 4.91372E+00 | 4.88281E-10 | 4.91372E+00 | 4.88281E-10 | 4.91372E+00 | 4.88281E-10 |
| 2.45686E+00 | 2.44140E-11 | 2.45686E+00 | 2.44140E-11 | 2.45686E+00 | 2.44140E-11 |
| 1.22843E+00 | 1.22070E-12 | 1.22843E+00 | 1.22070E-12 | 1.22843E+00 | 1.22070E-12 |
| 5.94217E-01 | 5.90350E-13 | 5.94217E-01 | 5.90350E-13 | 5.94217E-01 | 5.90350E-13 |
| 2.97108E-01 | 2.95175E-14 | 2.97108E-01 | 2.95175E-14 | 2.97108E-01 | 2.95175E-14 |
| 1.48554E-01 | 1.47587E-15 | 1.48554E-01 | 1.47587E-15 | 1.48554E-01 | 1.47587E-15 |
| 7.42772E-02 | 7.37937E-16 | 7.42772E-02 | 7.37937E-16 | 7.42772E-02 | 7.37937E-16 |
| 3.71386E-02 | 3.68968E-17 | 3.71386E-02 | 3.68968E-17 | 3.71386E-02 | 3.68968E-17 |
| 1.85693E-02 | 1.84484E-18 | 1.85693E-02 | 1.84484E-18 | 1.85693E-02 | 1.84484E-18 |
| 9.28467E-03 | 9.22420E-19 | 9.28467E-03 | 9.22420E-19 | 9.28467E-03 | 9.22420E-19 |
| 4.64234E-03 | 4.61210E-20 | 4.64234E-03 | 4.61210E-20 | 4.64234E-03 | 4.61210E-20 |
| 2.32117E-03 | 2.30605E-21 | 2.32117E-03 | 2.30605E-21 | 2.32117E-03 | 2.30605E-21 |
| 1.16058E-03 | 1.15302E-22 | 1.16058E-03 | 1.15302E-22 | 1.16058E-03 | 1.15302E-22 |
| 5.80292E-04 | 5.76511E-23 | 5.80292E-04 | 5.76511E-23 | 5.80292E-04 | 5.76511E-23 |
| 2.90146E-04 | 2.88255E-24 | 2.90146E-04 | 2.88255E-24 | 2.90146E-04 | 2.88255E-24 |
| 1.45073E-04 | 1.44127E-25 | 1.45073E-04 | 1.44127E-25 | 1.45073E-04 | 1.44127E-25 |
| 7.25366E-05 | 7.20614E-26 | 7.25366E-05 | 7.20614E-26 | 7.25366E-05 | 7.20614E-26 |
| 3.62683E-05 | 3.60307E-27 | 3.62683E-05 | 3.60307E-27 | 3.62683E-05 | 3.60307E-27 |
| 1.81341E-05 | 1.80153E-28 | 1.81341E-05 | 1.80153E-28 | 1.81341E-05 | 1.80153E-28 |
| 8.96705E-06 | 8.90767E-29 | 8.96705E-06 | 8.90767E-29 | 8.96705E-06 | 8.90767E-29 |
| 4.48352E-06 | 4.45383E-30 | 4.48352E-06 | 4.45383E-30 | 4.48352E-06 | 4.45383E-30 |
| 2.24176E-06 | 2.22691E-31 | 2.24176E-06 | 2.22691E-31 | 2.24176E-06 | 2.22691E-31 |
| 1.12088E-06 | 1.11345E-32 | 1.12088E-06 | 1.11345E-32 | 1.12088E-06 | 1.11345E-32 |
| 5.60444E-07 | 5.56722E-33 | 5.60444E-07 | 5.56722E-33 | 5.60444E-07 | 5.56722E-33 |
| 2.80222E-07 | 2.78361E-34 | 2.80222E-07 | 2.78361E-34 | 2.80222E-07 | 2.78361E-34 |
| 1.40111E-07 | 1.39180E-35 | 1.40111E-07 | 1.39180E-35 | 1.40111E-07 | 1.39180E-35 |
| 7.00556E-08 | 7.00900E-36 | 7.00556E-08 | 7.00900E-36 | 7.00556E-08 | 7.00900E-36 |
| 3.50278E-08 | 3.50450E-37 | 3.50278E-08 | 3.50450E-37 | 3.50278E-08 | 3.50450E-37 |
| 1.75139E-08 | 1.75225E-38 | 1.75139E-08 | 1.75225E-38 | 1.75139E-08 | 1.75225E-38 |
| 8.75695E-09 | 8.76112E-39 | 8.75695E-09 | 8.76112E-39 | 8.75695E-09 | 8.76112E-39 |
| 4.37848E-09 | 4.38056E-40 | 4.37848E-09 | 4.38056E-40 | 4.37848E-09 | 4.38056E-40 |
| 2.18924E-09 | 2.19028E-41 | 2.18924E-09 | 2.19028E-41 | 2.18924E-09 | 2.19028E-41 |
| 1.09462E-09 | 1.09514E-42 | 1.09462E-09 | 1.09514E-42 | 1.09462E-09 | 1.09514E-42 |
| 5.47311E-10 | 5.47572E-43 | 5.47311E-10 | 5.47572E-43 | 5.47311E-10 | 5.47572E-43 |
| 2.73656E-10 | 2.73786E-44 | 2.73656E-10 | 2.73786E-44 | 2.73656E-10 | 2.73786E-44 |
| 1.36828E-10 | 1.36993E-45 | 1.36828E-10 | 1.36993E-45 | 1.36828E-10 | 1.36993E-45 |
| 6.84144E-11 | 6.84967E-46 | 6.84144E-11 | 6.84967E-46 | 6.84144E-11 | 6.84967E-46 |
| 3.42072E-11 | 3.42483E-47 | 3.42072E-11 | 3.42483E-47 | 3.42072E-11 | 3.42483E-47 |
| 1.71036E-11 | 1.71241E-48 | 1.71036E-11 | 1.71241E-48 | 1.71036E-11 | 1.71241E-48 |
| 8.55181E-12 | 8.56205E-49 | 8.55181E-12 | 8.56205E-49 | 8.55181E-12 | 8.56205E-49 |
| 4.27591E-12 | 4.28102E-50 | 4.27591E-12 | 4.28102E-50 | 4.27591E-12 | 4.28102E-50 |
| 2.13795E-12 | 2.14051E-51 | 2.13795E-12 | 2.14051E-51 | 2.13795E-12 | 2.14051E-51 |
| 1.06898E-12 | 1.07025E-52 | 1.06898E-12 | 1.07025E-52 | 1.06898E-12 | 1.07025E-52 |
| 5.34492E-13 | 5.35125E-53 | 5.34492E-13 | 5.35125E-53 | 5.34492E-13 | 5.35125E-53 |
| 2.67246E-13 | 2.67562E-54 | 2.67246E-13 | 2.67562E-54 | 2.67246E-13 | 2.67562E-54 |
| 1.33623E-13 | 1.33781E-55 | 1.33623E-13 | 1.33781E-55 | 1.33623E-13 | 1.33781E-55 |
| 6.68116E-14 | 6.68900E-56 | 6.68116E-14 | 6.68900E-56 | 6.68116E-14 | 6.68900E-56 |
| 3.34058E-14 | 3.34450E-57 | 3.34058E-14 | 3.34450E-57 | 3.34058E-14 | 3.34450E-57 |
| 1.67029E-14 | 1.67225E-58 | 1.67029E-14 | 1.67225E-58 | 1.67029E-14 | 1.67225E-58 |
| 8.35145E-15 | 8.36112E-59 | 8.35145E-15 | 8.36112E-59 | 8.35145E-15 | 8.36112E-59 |
| 4.17572E-15 | 4.18056E-60 | 4.17572E-15 | 4.18056E-60 | 4.17572E-15 | 4.18056E-60 |
| 2.08786E-15 | 2.09028E-61 | 2.08786E-15 | 2.09028E-61 | 2.08786E-15 | 2.09028E-61 |
| 1.04393E-15 | 1.04704E-62 | 1.04393E-15 | 1.04704E-62 | 1.04393E-15 | 1.04704E-62 |
| 5.21969E-16 | 5.23520E-63 | 5.21969E-16 | 5.23520E-63 | 5.21969E-16 | 5.23520E-63 |
| 2.60985E-16 | 2.61760E-64 | 2.60985E-16 | 2.61760E-64 | 2.60985E-16 | 2.61760E-64 |
| 1.30492E-16 | 1.30880E-65 | 1.30492E-16 | 1.30880E-65 | 1.30492E-16 | 1.30880E-65 |
| 6.52461E-17 | 6.54400E-66 | 6.52461E-17 | 6.54400E-66 | 6.52461E-17 | 6.54400E-66 |
| 3.26230E-17 | 3.27200E-67 | 3.26230E-17 | 3.27200E-67 | 3.26230E-17 | 3.27200E-67 |
| 1.63115E-17 | 1.63600E-68 | 1.63115E-17 | 1.63600E-68 | 1.63115E-17 | 1.63600E-68 |
| 8.15575E-18 | 8.18000E-69 | 8.15575E-18 | 8.18000E-69 | 8.15575E-18 | 8.18000E-69 |
| 4.07788E-18 | 4.09000E-70 | 4.07788E-18 | 4.09000E-70 | 4.07788E-18 | 4.09000E-70 |
| 2.03894E-18 | 2.04500E-71 | 2.03894E-18 | 2.04500E-71 | 2.03894E-18 | 2.04500E-71 |
| 1.01947E-18 | 1.02250E-72 | 1.01947E-18 | 1.02250E-72 | 1.01947E-18 | 1.02250E-72 |
| 5.09736E-19 | 5.11250E-73 | 5.09736E-19 | 5.11250E-73 | 5.09736E-19 | 5.11250E-73 |
| 2.54868E-19 | 2.55625E-74 | 2.54868E-19 | 2.55625E-74 | 2.54868E-19 | 2.55625E-74 |
| 1.27434E-19 | 1.278125E-75 | 1.27434E-19 | 1.278125E-75 | 1.27434E-19 | 1.278125E-75 |
| 6.37170E-20 | 6.390625E-76 | 6.37170E-20 | 6.390625E-76 | 6.37170E-20 | 6.390625E-76 |
| 3.18585E-20 | 3.1953125E-77 | 3.18585E-20 | 3.1953125E-77 | 3.18585E-20 | 3.1953125E-77 |
| 1.59292E-20 | 1.59765625E-78 | 1.59292E-20 | 1.59765625E-78 | 1.59292E-20 | 1.59765625E-78 |
| 7.96461E-21 | 7.98828125E-79 | 7.96461E-21 | 7.98828125E-79 | 7.96461E-21 | 7.98828125E-79 |
| 3.98230E-21 | 3.994140625E-80 | 3.98230E-21 | 3.994140625E-80 | 3.98230E-21 | 3.994140625E-80 |
| 1.99115E-21 | 1.9970703125E-81 | 1.99115E-21 | 1.9970703125E-81 | 1.99115E-21 | 1.9970703125E-81 |
| 9.95575E-22 | 9.9853515625E-82 | 9.95575E-22 | 9.9853515625E-82 | 9.95575E-22 | 9.9853515625E-82 |
| 4.97788E-22 | 4.98767578125E-83 | 4.97788E-22 | 4.98767578125E-83 | 4.97788E-22 | 4.98767578125E-83 |
| 2.48894E-22 | 2.493837890625E-84 | 2.48894E-22 | 2.493837890625E-84 | 2.48894E-22 | 2.493837890625E-84 |
| 1.24447E-22 | 1.246918453125E-85 | 1.24447E-22 | 1.246918453125E-85 | 1.24447E-22 | 1.246918453125E-85 |
| 6.22235E-23 | 6.23459228125E-86 | 6.22235E-23 | 6.23459228125E-86 | 6.22235E-23 | 6.23459228125E-86 |
| 3.11117E-23 | 3.117296140625E-87 | 3.11117E-23 | 3.117296140625E-87 | 3.11117E-23 | 3.117296140625E-87 |
| 1.55559E-23 | 1.558648046875E-88 | 1.55559E-23 | 1.558648046875E-88 | 1.55559E-23 | 1.558648046875E-88 |
| 7.77795E-24 | 7.7933241796875E-89 | 7.77795E-24 | 7.7933241796875E-89 | 7.77795E-24 | 7.7933241796875E-89 |
| 3.88897E-24 | 3.89666208546875E-90 | 3.88897E-24 | 3.89666208546875E-90 | 3.88897E-24 | 3.89666208546875E-90 |
| 1.94449E-24 | 1.948331042734375E-91 | 1.94449E-24 | 1.948331042734375E-91 | 1.94449E-24 | 1.948331042734375E-91 |
| 9.72249E-25 | 9.741655213671875E-92 | 9.72249E-25 | 9.741655213671875E-92 | 9.72249E-25 | 9.741655213671875E-92 |
| 4.86124E-25 | 4.870827608935547E-93 | 4.86124E-25 | 4.870827608935547E-93 | 4.86124E-25 | 4.870827608935547E-93 |
| 2.43062E-25 | 2.435413804467773E-94 | 2.43062E-25 | 2.435413804467773E-94 | 2.43062E-25 | 2.435413804467773E-94 |
| 1.21531E-25 | 1.2177069022338865E-95 | 1.21531E-25 | 1.2177069022338865E-95 | 1.21531E-25 | 1.2177069022338865E-95 |
| 6.07656E-26 | 6.088533511169432E-96 | 6.07656E-26 | 6.088533511169432E-96 | 6.07656E-26 | 6.088533511169432E-96 |
| 3.03828E-26 | 3.044266755584716E-97 | 3.03828E-26 | 3.044266755584716E-97 | 3.03828E-26 | 3.044266755584716E-97 |
| 1.51914E-26 | 1.522133377792358E-98 | 1.51914E-26 | 1.522133377792358E-98 | 1.51914E-26 | 1.522133377792358E-98 |
| 7.59572E-27 | 7.61066688896179E-99 | 7.59572E-27 | 7.61066688896179E- | | |

| INPUT NO. | DATA | INPUT NO. |
|-----------|---|----------------------------|
| 66119-000 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 0. | 2.6919955000 -2.0496948000 |
| 66119-001 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 1. | 2.6919955000 -2.1218160000 |
| 66119-002 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 2. | 2.6919955000 -2.1939370000 |
| 66119-003 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 3. | 2.6919955000 -2.2660580000 |
| 66119-004 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 4. | 2.6919955000 -2.3381790000 |
| 66119-005 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 5. | 2.6919955000 -2.4103000000 |
| 66119-006 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 6. | 2.6919955000 -2.4824210000 |
| 66119-007 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 7. | 2.6919955000 -2.5545420000 |
| 66119-008 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 8. | 2.6919955000 -2.6266630000 |
| 66119-009 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 9. | 2.6919955000 -2.6987840000 |
| 66119-010 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 10. | 2.6919955000 -2.7709050000 |
| 66119-011 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 11. | 2.6919955000 -2.8430260000 |
| 66119-012 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 12. | 2.6919955000 -2.9151470000 |
| 66119-013 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 13. | 2.6919955000 -2.9872680000 |
| 66119-014 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 14. | 2.6919955000 -3.0593890000 |
| 66119-015 | COEFFICIENTS FOR FREQUENCY LEVEL NO. 15. | 2.6919955000 -3.3397370000 |

SECTION IV

EXAMPLE PROBLEM - F-4 STRESS SPECTRUM FOR POSITIVE LOAD FACTORS

The data base for this problem is four quarters of VGH data starting with the second quarter of 1972 and finishing with the first quarter of 1973. The VGH histogram intervals for these data are the following:

Indicated airspeed (knots)
150, 200, 250, 300, 350, 400, 450, 500, 550, 625, and
700

Normal load factor (equivalent)
1.4, 1.8, 2.2, 2.6, 3.0, 3.8, 4.6, 5.4, 6.6, 7.8, and 9.0

Altitude (feet)
0, 1000, 2000, 5000, 10,000, 15,000, 20,000, 30,000,
40,000, and 50,000

Weight (pounds)
37,500 (reference weight)

The stress table was set up with the following indicated airspeed, normal load factor, altitude, and weight combinations:

Indicated airspeed (knots)
175, 225, 275, 325, 375, 425, 475, 525, 575, and 625

Normal load factor
2.4, 2.8, 3.4, 4.2, 5.0, 6.0, 7.2, and 8.9

Altitude (feet)
500, 1500, 3500, 7500, 12500, 17500, 25000, and 35000

Weight (pounds)
37,500

The VGH histogram table was made up using all of the available data for the air-to-air and air-to-ground operations for the four quarters without distinguishing the various F-4 models except that only the unslatted configurations were considered. The numbers of hours of data in each category and their corresponding numbers of positive and negative load occurrences are shown in Table 1.

The number of stress exceedances per 1000 hours for load reference station (LRS) 180, defined in Figure 1 is shown in Figure 2 through Figure 7. Figure 2 through Figure 5 shows the variation from quarter to quarter of the VGH data. The stress exceedance graphs appear to show a small degree of scatter except for the SEA air-to-air first quarter where there was an overt change in the mission although it was still categorized as air-to-air. The four quarters of data are combined in Figures 6 and 7 to show the differences between the CONUS and SEA in the air-to-air operation and the air-to-ground operation.

SECTION V CONCLUSIONS

The procedure described in this report can eliminate much of the uncertainty that can occur in the derivation of the maneuver load stress spectrum. For new aircraft an estimate must be made of the VGH histogram to obtain the spectrum. This estimate can be updated during Task V of ASIP to derive a better estimate for the operational life of the fleet. This procedure can be immediately applied to fleet tracking by computing the conditional probability of exceeding a stress level given the normal load factor.

The application to full scale aircraft testing makes use of the assumption that the stress is matched at a specified number of control points by a linear combination of the same number of balanced loading conditions. This technique is believed to be more accurate than the usual process of a damage match at the specified control points in that the troublesome damage calculation is eliminated. The stress spectra at points other than control points are presumed to be matched satisfactorily by using representative loading conditions. It is, of course, theoretically better to use all points of the sky that occur in the VGH histogram. This, however, may be impractical due to test equipment limitations.

The procedure as applied to the F-4 fleet indicates that in general the stress spectra do not show significant changes from quarter to quarter. Also, when an operational change is made the method will reflect that change. When CONUS and SEA data are compared there appears to be a reasonably good correlation between the spectra generated in training and the spectra generated in combat.

TABLE 1. F-4 VGH DATA SUMMARY

| PERIOD | TYPE | HOURS | + COUNTS | - COUNTS | TOTAL COUNTS |
|--------|----------|---------|----------|----------|--------------|
| 2Q 72 | CONUS AA | 196.87 | 13981 | 4541 | 18522 |
| 2Q 72 | SEA AA | 65.84 | 4047 | 662 | 4709 |
| 2Q 72 | CONUS AG | 251.70 | 30723 | 9432 | 40155 |
| 2Q 72 | SEA AG | 1248.94 | 93027 | 13258 | 106285 |
| 3Q 72 | CONUS AA | 290.22 | 17470 | 5259 | 22729 |
| 3Q 72 | SEA AA | 393.26 | 30842 | 6366 | 37208 |
| 3Q 72 | CONUS AG | 469.64 | 38968 | 9934 | 48902 |
| 3Q 72 | SEA AG | 802.74 | 66446 | 12485 | 78931 |
| 4Q 72 | CONUS AA | 184.92 | 9404 | 3138 | 12542 |
| 4Q 72 | SEA AA | 164.35 | 7862 | 1933 | 9795 |
| 4Q 72 | CONUS AG | 89.16 | 5959 | 1265 | 7224 |
| 4Q 72 | SEA AA | 502.09 | 28254 | 4819 | 33073 |
| 1Q 73 | CONUS AA | 123.18 | 7983 | 2231 | 10214 |
| 1Q 73 | SEA AA | 133.96 | 6100 | 1358 | 7458 |
| 1Q 73 | CONUS AG | 194.38 | 17828 | 4001 | 21829 |
| 1Q 73 | SEA AG | 933.87 | 42342 | 8229 | 50571 |

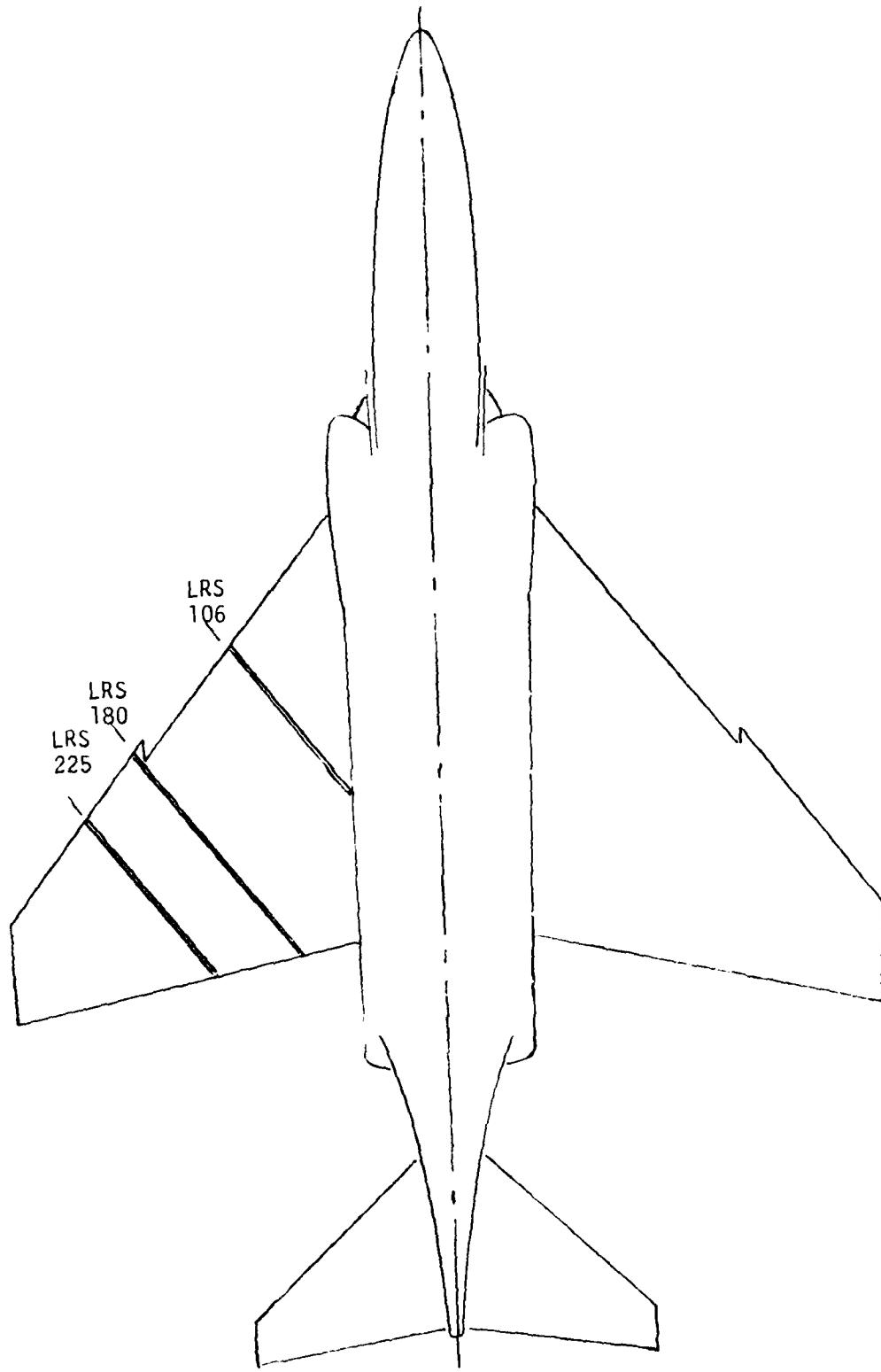


Figure 1. F-4 Wing Load Reference Station Locations

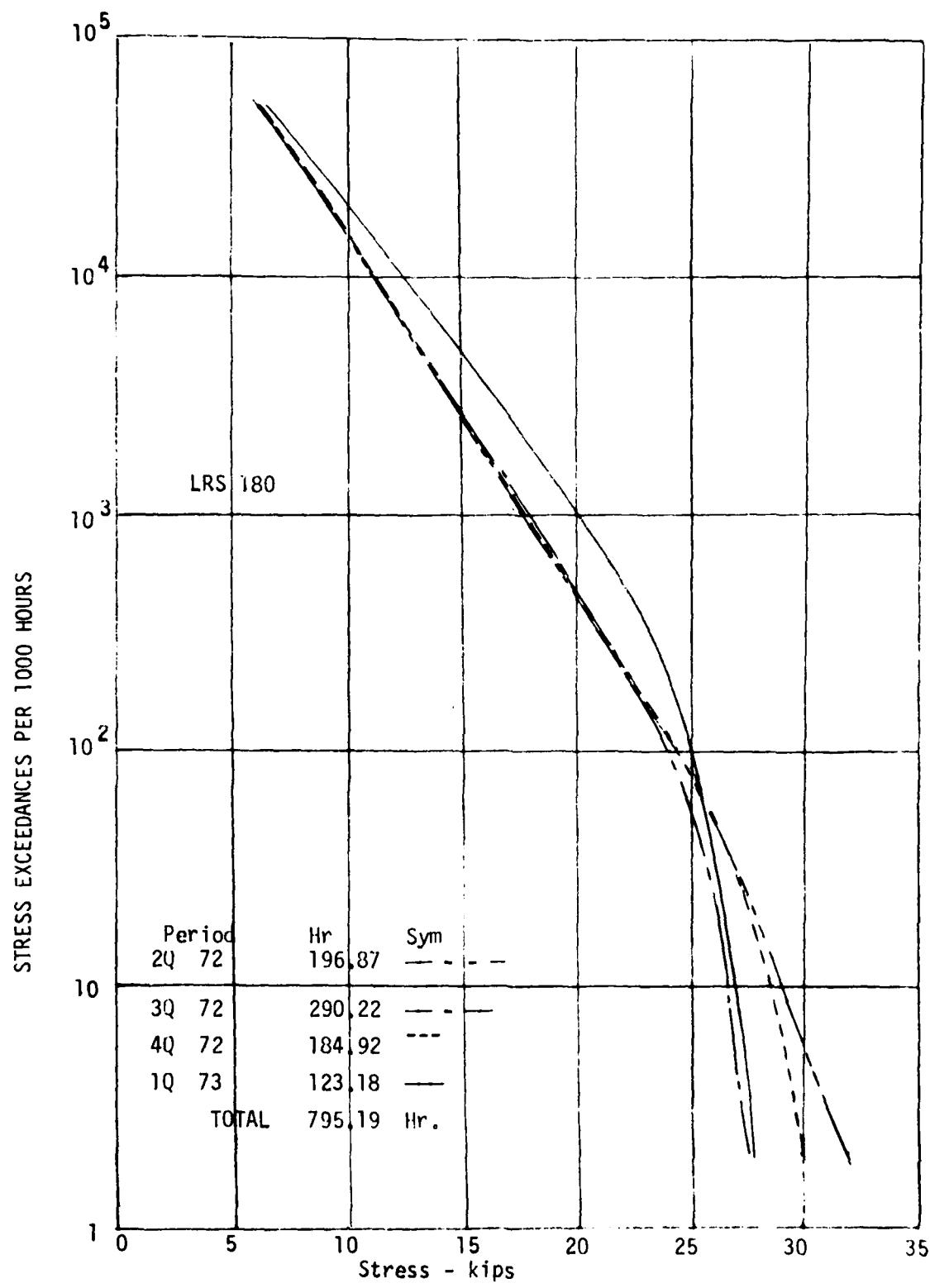


Figure 2. F-4 Spectra - CONUS Air-to-Air (All Models)

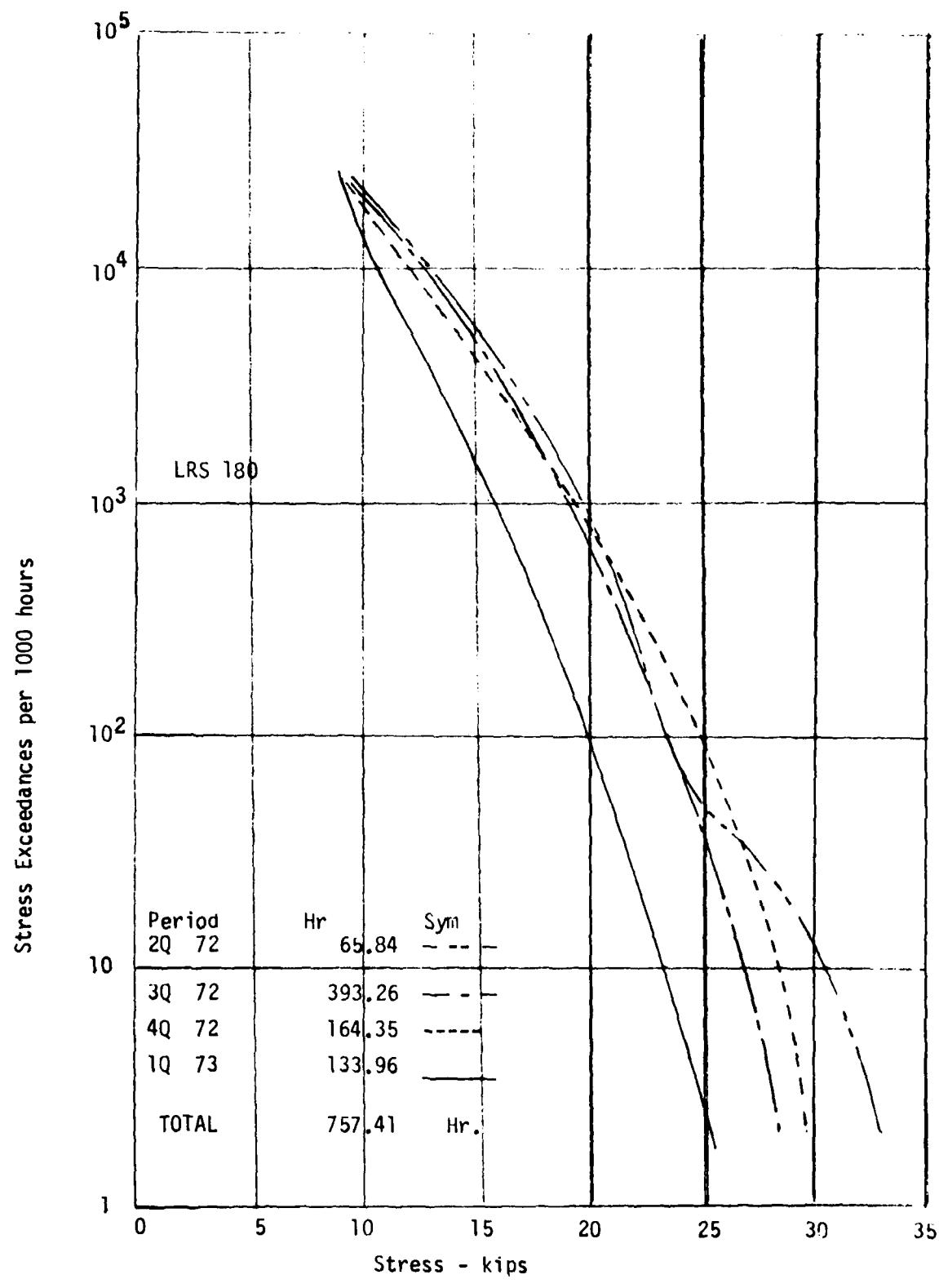


Figure 3. F-4 Spectra - SEA Air-to-Air (All Models)

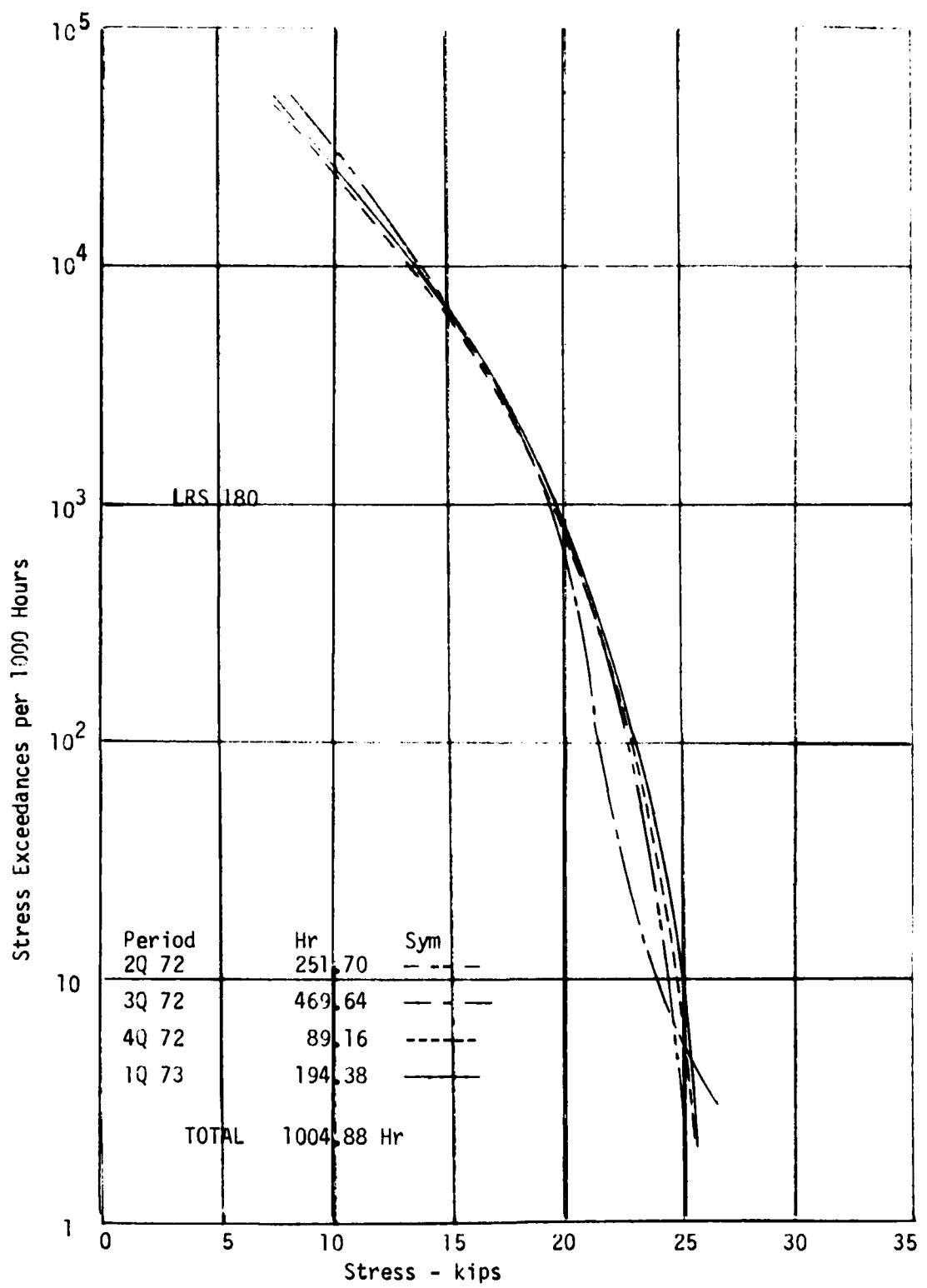


Figure 4. F-4 Spectra - CONUS Air-to-Ground (All Models)

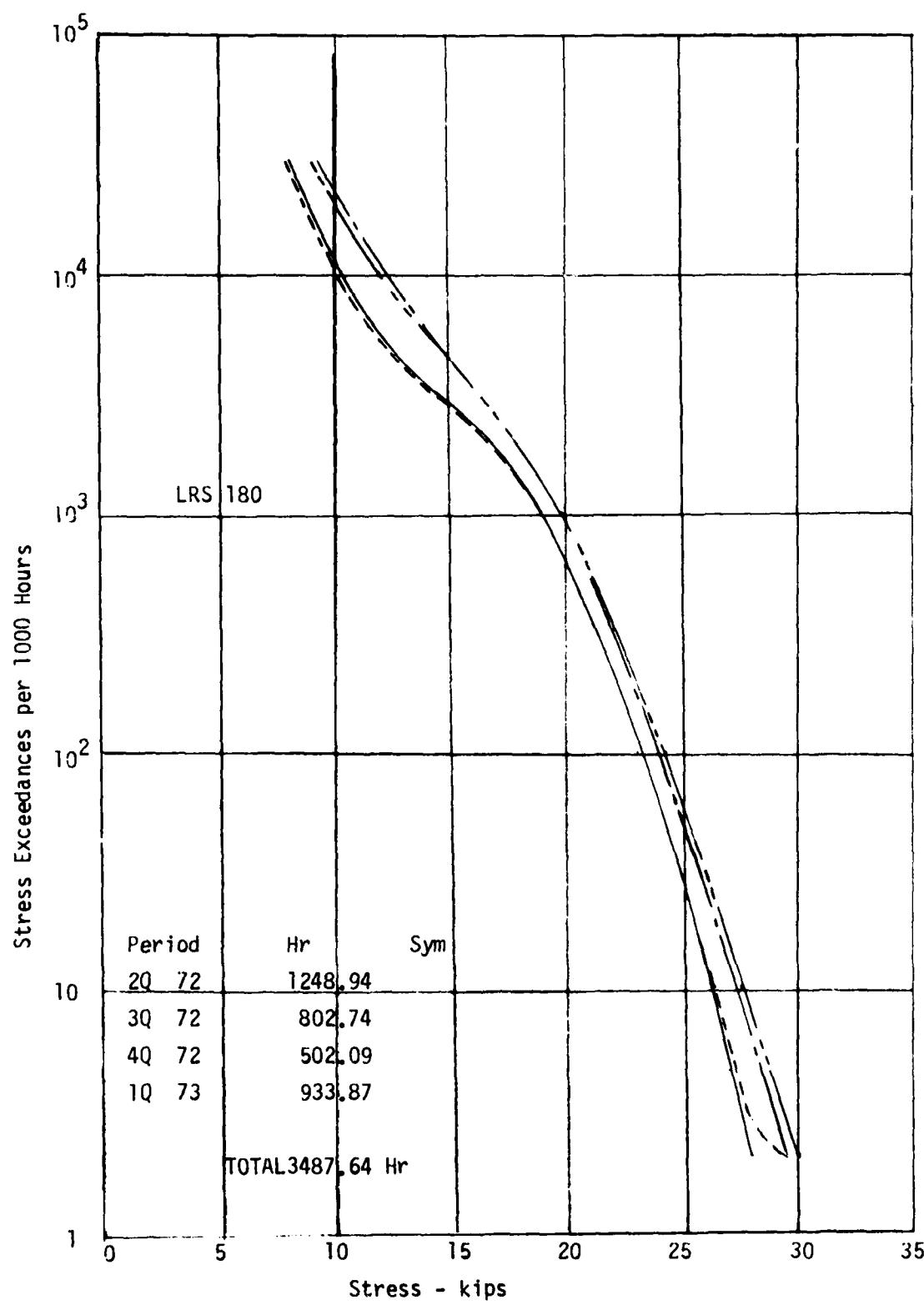


Figure 5. F-1 Spectra - SEA Air-to-Ground (All Models)

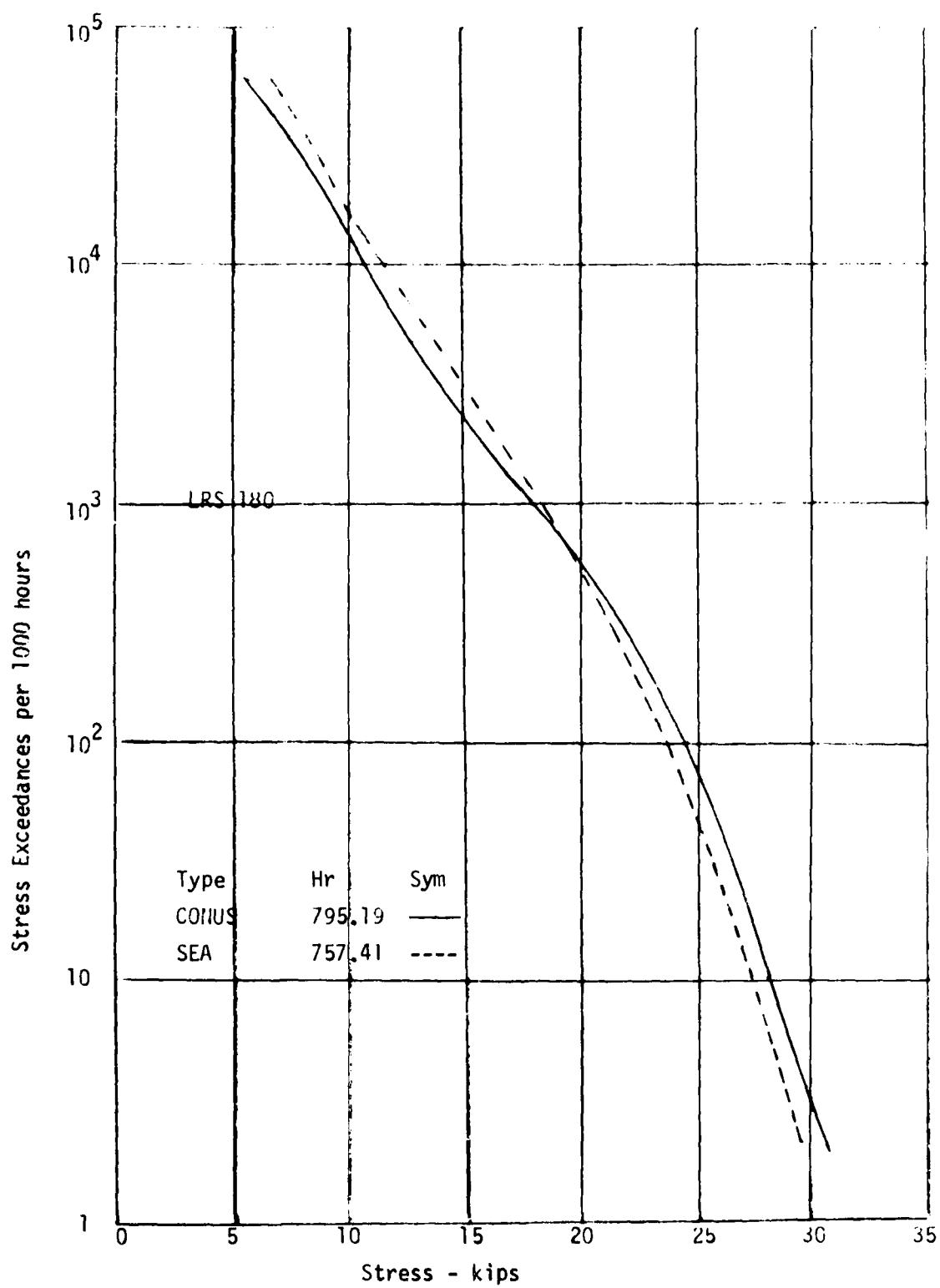


Figure 6. F-4 Spectra - Air-to-Air (All Models)
for One Year of VGH Data

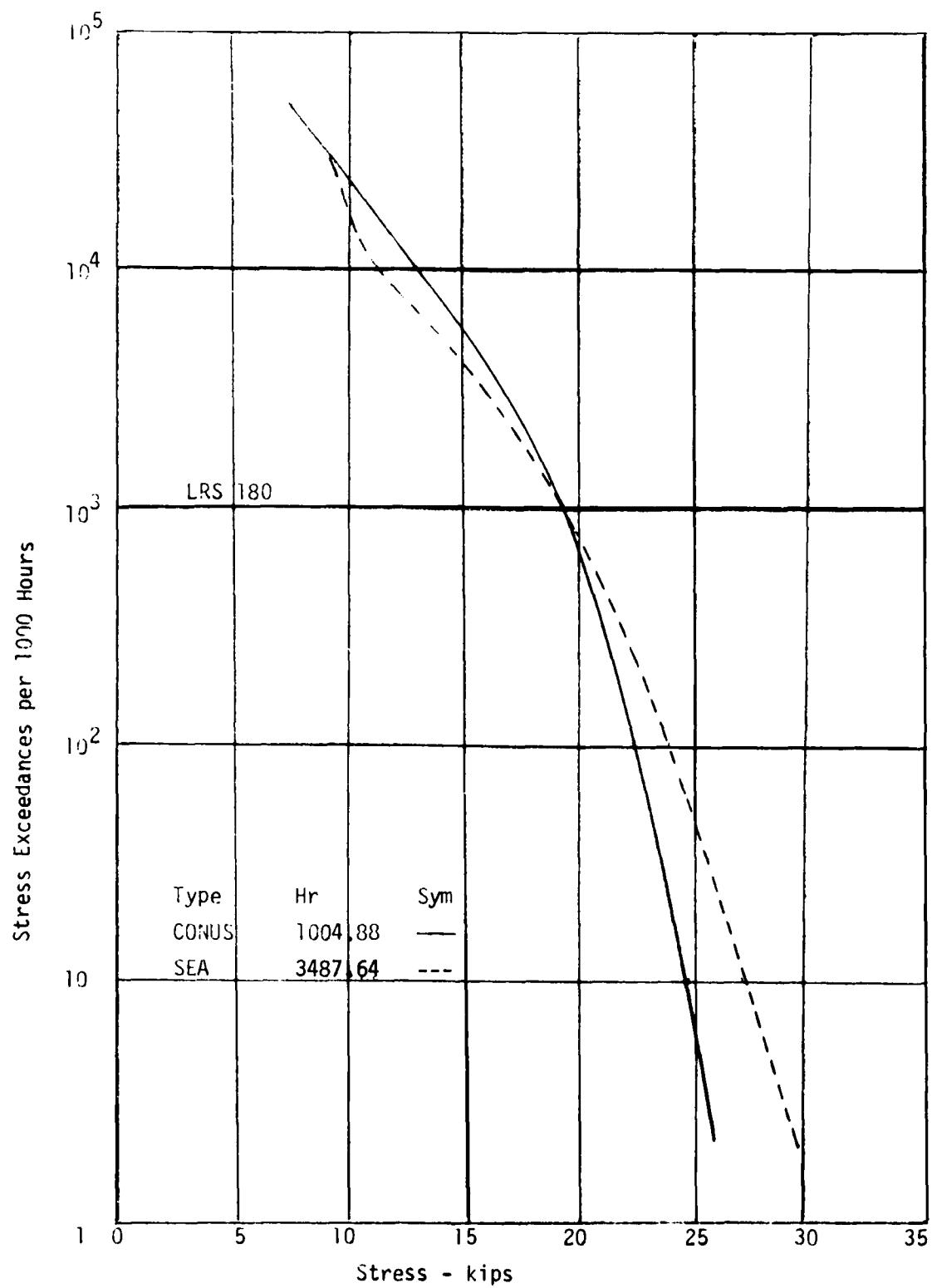


Figure 7. F-4 Spectra - Air-to-Ground (All Models)
for One Year of VGH Data

APPENDIX - SPECA PROGRAM LISTING

The listing given below is a FORTRAN extended language routine. This listing contains all of the statements for the version described in the Introduction of this report. Section 3.3 gives a brief description of each of the subroutines in this listing.

```
PROGRAM SPECIFY INPUT, OUTPUT, TAPE INPUT, TAPE OUTPUT  
C PROGRAM FOR COMPUTING AIRCRAFT INTERNAL LOAD PROBABILITY  
C DENSITY FUNCTIONS  
REVISION 2 COMMON P1100001, N11001001, T11001200, P1100001  
5      1 TA0121500.1) EQUIVALENCE (N11001001, NZERO), (N11001001, NPSET)  
      NZERO = 0  
      NPSET = 0  
      CALL GUIDF  
      GO TO 10  
      ENDF  
10      2L
```

SUBROUTINE GUIDE

PYTHON - 001

FTN 4.0+P553 - 11/02/73 09:55:14. - PAGE 1

C - SUBROUTINE FOR CALLING INPUT DATA AND CALCULATING ROUTINES
COMMON F10001, NTEGER100, TABLE4(2000,2),
C0VAL1NF (INTEGER13), MPSI
C0VAL1ME (INTEGER48), NZERO
C0VAL1NC (PYSI).
IF (NZERO) 40, 10
10
DO 20 I = 1, 10000
P113 = 0.0
DO 30 I = 1, 100
NIFGR11 = 0
GO TO 46
DO 40 I = 1001, 10000
P113 = 0.0
FACTOR = 1.0
CALL INPU
CALL CALC
CALL LDUL
CALL PRINTP
IF (INPT) 50, 60, 50
CALL LNOUT
RETURN
END

G10E 1
G10F 2
G10E 3
G10E 31
G10E 32
G10F 44
G10E 5
G10E 6
G10F 61
G10E 9
G10E 91
G11F 92
G10E 93
G10F 10
G10F 11
G10E 111
G10E 12
G10E 121
G10E 122
G10E 13
G10E 14

SUBROUTINE INPUT

INPUT

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```

      C   SUBROUTINE IN.   TABS, ARRAYS, AND TABLES   DEIN 1
      C   SUBROUTINE FOR INPUT OF   COMMON F10000, NTEGFR1000, TABLE42000,20.  DEIN 4
      C   YANL2500,11.   INTEGER MONTH   DEIN 5
      6   INTEGER MONTH   DEIN 51
      C   DIMENSION NTA43(21), NTB42(21), NTB43(21), NTA64(21)  DEIN 6
      C   EQUIVALENCE (P1930, MTB3)  DEIN 10
      C   EQUIVALENCE (NTEGER11, INENT1), (NTEGER12, NPF11).  DEIN 10
      C   EQUIVALENCE (NP11, NPF21), (INTEGER4, NP21), (INTEGER5, NP21).  DEIN 11
      C   EQUIVALENCE (NP12, NPF31), (INTEGER6, NP31), (INTEGER7, NP31).  DEIN 12
      C   EQUIVALENCE (NP13, NPF41), (INTEGER8, NP41), (INTEGER9, NP41).  DEIN 13
      C   EQUIVALENCE (NP14, NPF51), (INTEGER10, NP51), (INTEGER11, NP51).  DEIN 14
      C   EQUIVALENCE (NP15, NPF61), (INTEGER12, NP61), (NP61).  DEIN 15
      C   EQUIVALENCE (NP16, NPF71), (NP71).  DEIN 16
      C   EQUIVALENCE (NP17, NPF81), (NP81).  DEIN 17
      C   EQUIVALENCE (NP18, NPF91), (NP91).  DEIN 18
      C   EQUIVALENCE (NP19, NPF101), (NP101).  DEIN 19
      C   EQUIVALENCE (NP20, NPF111), (NP111).  DEIN 20
      C   EQUIVALENCE (NP21, NPF121), (NP121).  DEIN 21
      C   EQUIVALENCE (NP22, NPF131), (NP131).  DEIN 22
      C   EQUIVALENCE (NP23, NPF141), (NP141).  DEIN 23
      C   INPUT DATA   DEIN 204
      C   NTEGEN11 = IDENT - PROBLEM NUMBER   DEIN 211
      C   NTEGER12 = NP11 - THE NUMBER OF SETS OF DATA TO BE READ IN  DEIN 212
      C   BY FORMAT 1  DEIN 213
      C   NTEGEN13 = NP12 - THE NUMBER OF PARAMETERS TO BE READ IN  DEIN 214
      C   BY FORMAT 2  DEIN 215
      C   NTEGEN14 = NP13 - THE NUMBER OF SETS OF INTEGERS TO BE READ IN  DEIN 216
      C   READ IN BY FORMAT 3  DEIN 217
      C   NTEGEN15 = NP14 - NUMBER OF SETS OF INTEGERS TO BE READ IN  DEIN 218
      C   BY FORMAT 4  DEIN 219
      C   NTEGEN16 = NP15 - THE NUMBER OF QUADRUPLE TABLES TO BE READ  DEIN 220
      C   NTEGEN17 = NP16 - 1 FOR QUADRUPLE TABLE PRINT, 0 OTHERWISE  DEIN 221
      C   NTEGER11 = MONTH  DEIN 222
      C   NTEGEN18 = DAY  DEIN 223
      C   NTEGEN19 = YEAR  DEIN 224
      C   NTEGEN10 = NP51 - THE NUMBER OF INTERNAL LOAD LEVELS USED  DEIN 225
      C   FOR INTEGRATION OF JOINT DENSITY FUNCTION  DEIN 226
      C   INTERNAL LOAD SPECTRUM  DEIN 227
      C   NTEGEN11 = NP52 - NUMBER OF LOAD LEVELS IN THE  DEIN 228
      C   INTERNAL LOAD SPECTRUM  DEIN 229
      C   NTEGEN12 = NP53 - NUMBER OF CONTROL POINTS  DEIN 230
      C   NTEGEN13 = NPS - NUMBER OF ADDITIONAL INTEGERS PLUS 14  DEIN 231
      C   NTEGEN14 = NMORE - INDICATED AIRSPEED INTERVAL SUBDIVISION  DEIN 232
      C   NTEGEN15 = NRW1 - LOAD FACTOR INTERNAL SUBDIVISIONS  DEIN 233
      C   NTEGEN16 = NP51 - NRH - ALTITUDE INTERNAL SURVEYCTIONS  DEIN 234
      C   NTEGEN17 = NWR - NWI - WEIGHT INTERNAL SURVEYCTIONS  DEIN 235
      C   NTEGEN18 = NWT - NWB - 1 FOR QUADRUPLE TABLE LOOK UP CASE  DEIN 235
      C   NTEGEN19 = NWT - 2 FOR TRIPLE TABLE LOOK UP CASE  DEIN 235
      C   P(1) - FV1 - LEAST UPPER BOUND OF V1 IN HISTOGRAM  DEIN 236
      C   P(2) - FN1 - LEAST UPPER BOUND OF N2 IN HISTOGRAM  DEIN 236
      C   P(3) - FM - LEAST UPPER BOUND OF M IN HISTOGRAM  DEIN 236
      C   P(4) - FW - LEAST UPPER BOUND OF W IN HISTOGRAM  DEIN 236
      C   P(5) - FACTOR - LOAD MAGNIFICATION FACTOR  DEIN 236
      C   P(6) - HOURS - NUMBER OF HOURS OF DATA IN HISTOGRAM  DEIN 236
      C   P(101) - PSIL111 - FIRST LOAD LEVEL FOR PROBABILITY CALC.  DEIN 236
      C   P(201) - AREAN11 - FIRST OPO. OF CUM. PROC. FUNC. FOR SPEC.  DEIN 236
      C   IF (NHS > 10, 10, 2)  DEIN 236
      C   NPAGF = NPAGF + 1  DEIN 237
      C   GO TO 3C  DEIN 238
      C   NPAGF = 1  DEIN 238
      C   READ INTEGERS INTO THE PRCBLEM  DEIN 238
      C   2  DEIN 238
      C   11  DEIN 238
      C   C

```

SUSTAINABILITY

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SUBROUTINE INPUT

MAIN -OPT=1

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```
      115          READ (5,140) (TANL4(K,I), K = 1, NTT4)
      READ (5,140) (TANL6(K,I), K = NTT1P1, NNTT12)
      READ (5,140) (TANL6(K,I), K = NTT1P1,
      GO TO (654,656), J
      GO TO (656,660), K10
      READ (5,140) (TANL4(K,I), K = NNT13P1, NNTT14)
      READ (5,140) (TANL4(K,I), K = NNT13P1,
      GO TO 670
      READ (5,140) MTB3
      NF = NNT13 + NTP
      READ (5,140) (TANL6(K,I), K = NN13P1, NF)
      CONTINUE
      CALL INIC
      RETURN
      END
```

125

115

654

656

660

K10

J

DEFIN104

DEFIN105

DEFIN106

DEFIN107

DEFIN108

DEFIN109

DEFIN110

DEFIN111

SUBROUTINE: MAIN : 74376 , DPT=1
FIN 4.8.8361 ----- 11/92/71 - 09.05.22. - PAGE - 3

```
      TON, 0.0PNZ • E15.6 /   INAO 67
      10, 0PNH = 0 E15.6 /   INAO 68
      10, 0PNW = 0 E15.6 /   INAO 69
      NZERO = 1               INAO 90
      RETURN
      END
      120
```



```

      1000      SUBROUTINE L0LV
      1001      C   SUBROUTINE FOR COMPUTING INTERNAL LOAD LEVELS FOR
      1002      C   A GIVEN DISTRIBUTION OF LOAD CYCLES
      1003      C   COMMON P410000, NTECFR1001, JABLA4(2000,-20)
      1004      C   TANT12500,10
      1005      C   DIFUNSTN PPS11001, AP0PS11001, AP0PS11001
      1006      C   PS1L1001, PS1L1001, FRAC1001
      1007      C   EQUIVALENCE (P1101), PS1L1001
      1008      C   EQUIVALENCE (P11201), PS1L1001
      1009      C   EQUIVALENCE (P11301), PS1L1001, PP1L1001
      1010      C   EQUIVALENCE (P11401), FRAC1
      1011      C   EQUIVALENCE (TNECFR1111), NPSSILL10
      1012      C   NPSSILL10 = PS1L1001 - PS1L1001
      1013      C   NO 10 J= 1, NPSSILL10
      1014      C   AP0PS11001 = 1.0 + PP1L1001
      1015      C   IF (ARFAN111 - AP0PS11001) 20, 50, 50
      1016      C   WRITE (16,30)
      1017      C   FORMAT (10X, 4HEWQCR MESSAGE - ARFAN111 LESS THAN AP0PS11001)
      1018      C   CALL PRTR
      1019      C   IF (ARFAN1NPSSILL10 - AP0PS11NPSSILL10) 90, 90, 60
      1020      C   WRITE (16,70)
      1021      C   FORMAT (10X, 5HERRCR MESSAGE - ARFAN1NPSSILL10 GREATER THAN AP0PS11NPSSILL10)
      1022      C   CALL PRINTR
      1023      C   DO 180 J = 1, NPSSILL10
      1024      C   DO 170 I = 1, NPSSILL10
      1025      C   IF (ARFAN1IJ - AP0PS11IJ) 110, 100, 170
      1026      C   PS1L1IJ = PS1L1IJ
      1027      C   GO TO 180
      1028      C   IF (I-11, 120, 120, 130
      1029      C   P1 = AP0PS1111
      1030      C   P2 = AP0PS1121
      1031      C   P3 = AP0PS1131
      1032      C   GO TO 140
      1033      C   P1 = AP0PS1111
      1034      C   P2 = AP0PS1121
      1035      C   P3 = AP0PS1131
      1036      C   4 = 0.5 * P1 - P2 + 0.5 * P3
      1037      C   B = -0.5 * P1 + 0.5 * P3
      1038      C   C = P2 - ARAN1IJ
      1039      C   DISC = B * C**2 - 4.0 * A.* C
      1040      C   IF (DISC) 140, 144, 146
      1041      C   WRITE (6,143) DISC
      1042      C   GO TO 140
      1043      C   FORMAT (10X, 6HDISC = F15.6)
      1044      C   CALL PRINTR
      1045      C   EIA = 1 - 0 + SQR(1NSILL1) / 12.0 * A1
      1046      C   IF (I-11-150, 150, 160, 160)
      1047      C   PS1L1IJ = PS1L1IJ + EIA * DELTA
      1048      C   GO TO 160
      1049      C   PS1L1IJ = PS1L1IJ + EIA * DELTA
      1050      C   GO TO 160
      1051      C   CONTINUE
      1052      C   NPP = NPSSILL10
      1053      C   FRAC10 = (ARFAN111 + ARFAN121) / 2.0
      1054      C   DC = 190, 1, 2, K2
      1055      C   FRAC11 = (ARFAN111 - ARFAN112) / 2.0
      1056      C   FRAC11NPSSILL10 = 1.0 - (ARFAN1NPSSILL10 +
      1057      C   FRAC11NPSSILL10) / 2.0
      1058      C   GO TO 160
      1059      C   END

```

SUBROUTINE LDVLN 7474 DPIT=1

FIN 4. SEP 1973 1102773-9.05.33 PAGE 2

1 AREANINPSILL-III / 2.0

RETURN

END

60

LDLV 458

LDLV 46

LDLV 47

ROUTINE LDCOF

7470

PIN 6.0+P53

11/02/73

09.05.56.

PAGE 1

C SUBROUTINE LDCOF
FOR COMPUTING THE LOAD CONDITION COEFFICIENTS
COMMON P100001, M1001001, TAME(2000,20),
DIMENSION DSILL(1000), PS125(25), ALPHAI(25),
PL0425(25), PL04251, ALPHAI(25),
EQUIVALENCE (R1001,PS1), (P11301,PS1LL),
(P11501,ALOMA),
EQUIVALENCE (NEGLR121, NPS1LL), (INTEGER131, NPS1),
(REALR1631, NNGL), (NEGLR1501, NPSCT),
NPSCT = NPSCT + 1
DC 10 I = 1, NPS1LL
PL04251 = PS1LL110
IF (NPS1 - NPS1) 130, 20,
DO 50 I = 1, NPS1
DO 50 J = 1, NPS1
ALI(J,I) = F51(I,J)
JNPS1 * J * NPS1
IF (I1 - J1) 40, 30, 40
ALI(JNP1) = 1.0
GO TO 50
ALI(JNP1) = 0.0
CONTINUE
CALL GAUS21(NPS1, NPS1, 1.0E-07, A, AJNW, K31)
IF (K3 = 11 60, 75, 60
NATR 66, 70, K3
FORMAT (10X, 2HGAUS21, ERNO SIGNAL - KJ = , I3)
NPAF = NFAGE + 1
CALL PACF0
DO 120 I = 1, NPS1LL
DO 60 J = 1, NPS1
PL04251 = PL0425(I,J)
DO 90 K = 1, NPS1
ALPHAK1 = Q, C
Q = 90 L = 1, NPS1
ALPHAK1 = ALPHIK1 + PL0425(I,J) * ALPHAI(K)
WITE (6,10) 1
FORMAT (1/10Y, 36HCOEFFICIENTS FOR FREQUENCY LEVEL NO. , IS 1
WITE (6,1101) (ALPHAI(I), TA = 1, NPS1
CONTINUE
120 FORMAT (1P815.6)
120 RETURN
END

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FIN 4009353

11/02/13 09:05 AM

```

      1 TABLE(112) = TABLE(112-11)
      1 X3DAT = X3DAT - TABLE(113-11) /          QTAB 58
      1 TABLE(113) = TABLE(113-11)               QTAB 59
      1 X4DAT = X4DAT - TABLE(114-11)               CTAB 60
      1 (TABLE(111) - TABLE(111-11)) * KIRAT * (TABLE(11211) - QTAB 61
      1 TABLE(111) * TABLE(111-11) * KIRAT * (TABLE(11211) - QTAB 62
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 63
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 64
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 65
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 66
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 67
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 68
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 69
      1 TABLE(11111) * KIRAT * (TABLE(11211) - QTAB 70
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 71
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 72
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 73
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 74
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 75
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 76
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 77
      1 TABLE(11112) = TABLE(11112) + KIRAT * (TABLE(11212) - QTAB 78
      1 TABLE(11112) = AMP111 + X2RAT * JAMP211 * AMF1111 - QTAB 79
      1 AMP111 = AMP111 + X2RAT * (AMP221 - AMP121) - QTAB 80
      1 AMP112 = AMP112 + X2RAT * (AMP212 - AMP121) - QTAB 81
      1 AMP112 = AMP112 + X2RAT * (AMP222 - AMP122) - CTAB 82
      1 AMP1 = AMP111 + X2RAT * (AMF211 - AMP111) - QTAB 83
      1 AMP2 = AMP112 + X2RAT * (AMF212 - AMP121) - QTAB 84
      1 AMP2 = AMP112 + X2RAT * (AMP22 - AMP121) - QTAB 85
      1 AMP = AMP1 + XLSAT * (AMP2 - AMP1) - QTAB 86
      RETURN
      ENO
      QTAB 87

```

SUBROUTINE PAGEID

JAN74

— OPT14 — FIN.4.062153 — 11/02/23 09:05:51. — PAGE 1

```
C      SUBROUTINE PAGEID  PAGH 1
      COMMON P100001, M1GEN1001, TANL47000.20,          PAGH 2
      TABLE250001
      5      INTEGER DAY, YFAD, IDENT1, IDENT2, MONTH1,      PAGH 3
              EQUIVALENCE IDENT1, IDENT2, MONTH1,          PAGH 4
              IDENT1, IDENT2, YEAR1, IDENT2, M1GEN1001,      PAGH 5
              WRITE(16,201) IDENT1, MONTH, DAY, YFAD, NPAGE      PAGH 6
              20      FORMAT(1X,0X,6HRUN NO., 16, 10X, 4HDATE, 14, 1W, 12,      PAGH 7
              10      10X, 7PAGE NO., 16)      PAGH 8
              14      RETURN      PAGH 9
              END      PAGH 10
              .      PAGH 11
              .      PAGH 12
              .      PAGH 13
              .      PAGH 14
```

SUBROUTINE GAUSS2 — 762a

OPTION — FIN A-B-A253 — 11/22/73 — 89.05.5a — PAGE — 1 —

GAUSS2(M,EP,A,X,K,N)

DIMENSION A(3,4), X(3,1)

NPM=4*M

L=1,N

KP=0

R=0.0

DO 1,2 K=L,N

16 17 ANS=(A(K,L))11,12,12

18 DO 1,2 K=L,N

19 20 KPA=

21 CONTINUE

22 R=(L-KP)13*20,20

23 DO 1,4 J=L,NPM

24 Z=A(L,J)

25 A(L,J)=A(KP,J)

26 A(KP,J)=2

27 T=(L-S)11,12,-EP150,50,30

28 IF ((L-S)31,40,40

29 LP1=L+1

30 DO 34 K=LP1,N

31 T=(L-K,LP1,LP1)

32 IF ((L-K,L)32,36,32

33 Q=(L-K,L)31,NPM

34 A(K,LP1,J)=RATIO(LP1,J)

35 CONTINUE

36 DO 43 I=1,N

37 IF (I=1,1)

38 P=M-J+1,N

39 S=0,1

40 IF (I=1-NB41+63,43

41 LP1=1,I+1

42 DO 42 K=LP1,N

43 S=(A(I,J)-A(Y,XA,J))/

44 X(I,J),A=(A(I,JPN)-S)/(A(I,JPN))

45 NR=1

46 GO TO 75

47 NR=2

48 CONTINUE

49 RETURN

50 ENO

51 GAUS 001

52 GAUS 002

53 GAUS 003

54 GAUS 004

55 GAUS 005

56 GAUS 006

57 GAUS 007

58 GAUS 008

59 GAUS 009

60 GAUS 010

61 GAUS 011

62 GAUS 012

63 GAUS 013

64 GAUS 014

65 GAUS 015

66 GAUS 016

67 GAUS 017

68 GAUS 018

69 GAUS 019

70 GAUS 020

71 GAUS 021

72 GAUS 022

73 GAUS 023

74 GAUS 024

75 GAUS 025

76 GAUS 026

77 GAUS 027

78 GAUS 028

79 GAUS 029

80 GAUS 030

81 GAUS 031

82 GAUS 032

83 GAUS 033

84 GAUS 034

85 GAUS 035

86 GAUS 036

87 GAUS 037

88 GAUS 038

89 GAUS 039

SUBROUTINE GAUS21 — 2676 — OPT1 — FIN 4-JAP1911 — 11/22/73 — 09:05:41. — PAGE — 1 —

```
      SUBROUTINE GAUS21(M,N,EP,AV,KERB)
      DIMENSION A(125,20), X(125,25)
      NEM144M
      M=1
      N=34 L=1,N
      MP=0
      Z=0,0
      10 12 KAL,M
      IF (Z>ANS) GOTO 11,12,13
      11 2=185 (A(L,K,L))
      12 K=P=X
      13 CONTINUE
      IF (L-KP1) 3,20,20
      14 16 J=L,NPM
      15 17 A(L,J)=A(L,P,J)
      16 A(L,P)=2
      17 E145*(A(L,L))-EP150+50,30
      18 19 T=(L-K)3,40,40
      20 21 T=(L-K)3,40,40
      22 23 A(L)=1
      24 25 A(L)=0
      26 27 0,34 K=L,P1,N
      28 29 K=L,P1,N
      30 31 K=L,P1,N
      32 33 K=L,P1,N
      34 35 K=L,P1,N
      36 37 K=L,P1,N
      38 39 K=L,P1,N
      40 41 K=L,P1,N
      42 43 K=L,P1,N
      44 45 K=L,P1,N
      46 47 K=L,P1,N
      48 49 K=L,P1,N
      50 51 K=L,P1,N
      52 53 K=L,P1,N
      54 55 K=L,P1,N
      56 57 K=L,P1,N
      58 59 K=L,P1,N
      60 61 K=L,P1,N
      62 63 K=L,P1,N
      64 65 K=L,P1,N
      66 67 K=L,P1,N
      68 69 K=L,P1,N
      70 71 K=L,P1,N
      72 73 K=L,P1,N
      74 75 K=L,P1,N
      76 77 K=L,P1,N
      78 79 K=L,P1,N
      80 81 K=L,P1,N
      82 83 K=L,P1,N
      84 85 K=L,P1,N
      86 87 K=L,P1,N
      88 89 K=L,P1,N
      90 91 K=L,P1,N
      92 93 K=L,P1,N
      94 95 K=L,P1,N
      96 97 K=L,P1,N
      98 99 K=L,P1,N
      100 101 K=L,P1,N
      102 103 K=L,P1,N
      104 105 K=L,P1,N
      106 107 K=L,P1,N
      108 109 K=L,P1,N
      110 111 K=L,P1,N
      112 113 K=L,P1,N
      114 115 K=L,P1,N
      116 117 K=L,P1,N
      118 119 K=L,P1,N
      120 121 K=L,P1,N
      122 123 K=L,P1,N
      124 125 K=L,P1,N
      126 127 K=L,P1,N
      128 129 K=L,P1,N
      130 131 K=L,P1,N
      132 133 K=L,P1,N
      134 135 K=L,P1,N
      136 137 K=L,P1,N
      138 139 K=L,P1,N
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      783 784 K=L,P1,N
      784 785 K=L,P1,N
      785 786 K=L,P1,N
      786 787 K=L,P1,N
      787 788 K=L,P1,N
      788 789 K=L,P1,N
      789 790 K=L,P1,N
      790 791 K=L,P1,N
      791 792 K=L,P1,N
      792 793 K=L,P1,N
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      795 796 K=L,P1,N
      796 797 K=L,P1,N
      797 798 K=L,P1,N
      798 799 K=L,P1,N
      799 800 K=L,P1,N
      800 801 K=L,P1,N
      801 802 K=L,P1,N
      802 803 K=L,P1,N
      803 804 K=L,P1,N
      804 805 K=L,P1,N
      805 806 K=L,P1,N
      806 807 K=L,P1,N
      807 808 K=L,P1,N
      808 809 K=L,P1,N
      809 810 K=L,P1,N
      810 811 K=L,P1,N
      811 812 K=L,P1,N
      812 813 K=L,P1,N
      813 814 K=L,P1,N
      814 815 K=L,P1,N
      815 816 K=L,P1,N
      816 817 K=L,P1,N
      817 818 K=L,P1,N
      818 819 K=L,P1,N
      819 820 K=L,P1,N
      820 821 K=L,P1,N
      821 822 K=L,P1,N
      822 823 K=L,P1,N
      823 824 K=L,P1,N
      824 825 K=L,P1,N
      825 826 K=L,P1,N
      826 827 K=L,P1,N
      827 828 K=L,P1,N
      828 829 K=L,P1,N
      829 830 K=L,P1,N
      830 831 K=L,P1,N
      831 832 K=L,P1,N
      832 833 K=L,P1,N
      833 834 K=L,P1,N
      834 835 K=L,P1,N
      835 836 K=L,P1,N
      836 837 K=L,P1,N
      837 838 K=L,P1,N
      838 839 K=L,P1,N
      839 840 K=L,P1,N
      840 841 K=L,P1,N
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SHARQUSINE PRINTER

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OPT1

FIN. A.43213

PAGE 2

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MPAGE 8. MPAGE 3.  
CALL PAGE0  
60 WRITE 16,00  
WHITE 16,00  
FORMAT1/101. 2MHCYCLIC LOADING, FRACTIONS.)  
WRITE (6,70)  
70 FORMATS (15P, UNLOAD, 5X, UNLOAD, 5X,  
ANFAC10CK, 19X, ANLOAD, 5X, UNFAC10CK)  
DO 80 I = 1, MPSILL, 3  
11 = 1, 1  
12 = 1, 2  
WRITE (46,30) MPSILL1, MPSILL2, MPSILL3,  
80 MPSILL123, HYAC121  
I MPSILL (6,50) NT  
70 FORMAT1/101, 19-INITIAL LOAD CYCLES =, F12.00  
RETURN  
END  
PONI 61
```